# 堆焊快速成形低碳钢件的裂纹形成机理

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摘 要:采用 \$\text{\$\text{EM}}\makebox{观察了堆焊快速成形低碳钢件的裂纹微观形貌. 结果表明,裂纹萌 生于成形件的初始沉积层,沿沉积高度方向扩展,终止于成形件表面之下,采用OM和 EDS分析了成形件中的偏析与夹杂物成分,利用 XRD分析了成形件中的残余奥氏体含 量,成形件中的裂纹为液化热裂纹,在多层多道连续堆焊成形过程中,Mn. Si的氧化物、 M的碳化物以及 N 金属间化合物的偏析是裂纹形成的内因,拉应力是裂纹形成的外 因. 通过合理匹配  $M_n$   $N_i$  S元素的含量,添加稀土元素 C净化焊缝金属,采用层层正 交的路径沉积,延长层间隔时间,可以消除堆焊快速成形低碳钢件的裂纹.

关键词: 堆焊: 快速成形: 金属芯焊丝: 裂纹: 偏析

中图分类号: TG142 文献标识码: A 文章编号: 0253-360X(2010)09-0053-04



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#### 0 序 言

焊接快速成形技术是基于离散 堆积的原理,通 过三维实体扫描或直接建模获得三维实体模型,将 模型沿某一坐标方向按一定的厚度进行分层切片处 理,然后由焊接热源将金属丝材(粉末)熔化,按设 定的成形路径堆积成形每一薄层,由层层堆积最终 形成全焊缝金属零件的先进制造技术, 可见, 焊接 快速成形技术是一种典型的分层制造技术, 焊接快 速成形技术具有制造成本低、生产效率高、制造形式 灵活、成形件性能好等优点[12].按照快速成形所采 用的焊接工艺分类、焊接快速成形技术可分为熔化 极气体保护焊、钨极气体保护焊、微弧等离子焊、激 光束焊、电子束焊等. 其中,基于熔化极气体保护焊 的堆焊快速成形技术在大尺寸金属零件的快速制 造 再制造成形方面具有显著的优势.

堆焊快速成形过程中, 若成形材料、工艺参数或 者路径规划的选择不当,可能导致成形件产生裂纹, 裂纹一旦产生,将沿着沉积层不断扩展,严重影响成 形件的性能,导致成形件报废[34].可见,对堆焊快 速成形过程中裂纹形成机理的研究具有重要意义. 为此,采用微观测试分析的方法,深入研究了以 Fe Mn\_SiNiMo系微渣型金属芯焊丝作为成形材料时 成形件的裂纹形成机理,并提出了减少或消除成形

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件裂纹的方法,为消除堆焊快速成形过程中成形件 的裂纹产生提供理论依据.

### 1 试验方法

采用装备再制造技术国防科技重点实验室开发 的"基于机器人的 MIG/MAG堆焊熔敷快速成形系 统",该系统集成了可离线编程控制的 ABB机器人 和 Fronius TPS4000型 MIG/MAG焊接系统. 焊接工 艺参数为送丝速度 5.0 m/m p,电弧电压 23.2 ~ 24.3 Ⅴ焊接电流 130~140 A焊接速度 10 mm/,\$ 焊丝伸出长度 10~15 mm,保护气体 80% A+20% ○○, 气体流量 18~20 L/m in 基板采用 200 mm× 100 mm×8 mm的 Q235 钢. 堆焊成形材料为自制 的金属芯焊丝,直径 1.2 mm,熔敷金属主要成分(质 量分数, %)为 (0, 08 Siq 33, Mrg 57, Mrg 44, N2 33 Fe余量.

按照"弓"字形轨迹逐层进行扫描,连续堆焊 8 层, 制备的成形件尺寸为 120 mm×60 mm×15 mm. 采用电火花线切割将成形件的 A截面切开, A截面 的宏观裂纹如图 1所示,然后将试样磨平、抛光,经 5%硝酸酒精溶液刻蚀后,采用 ○ [ympus IMG 3型金 相显微镜和 Quanta 200型环境真空扫描电镜观察试 样裂纹的微观形貌:采用 EDAX Genesi型能谱仪分 析试样中的偏析和夹杂物的成分: 采用 D8 AD-VANCE型 X射线衍射仪分析成形件中的残余奥氏 体的含量.

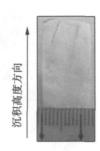
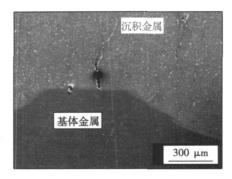


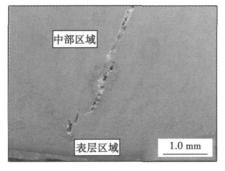
图 1 裂纹的宏观形貌 Fig 1 Macroscopic morphopgy of cracks

### 2 裂纹形成机理分析

采用扫描电镜观察图 1 所示的裂纹微观形貌如图 2 所示. 结合图 1 可见, 裂纹萌生于成形件的初始沉积层, 沿沉积高度方向不断扩展, 终止于成形件表面之下, 表面无裂纹出现.



(a) 裂纹形成区域



(b) 裂纹终止区域

图 2 裂纹的微观形貌 Fg 2 Micromorphopgy of cracks

图 3表明了裂纹形成与偏析、夹杂物的关系.由图 3可见,偏析是裂纹形成的前因,裂缝形成后,部分偏析成分形成夹杂物并聚集于裂缝之中. 在裂缝扩展受阻改变方向后,裂纹沿产生偏析的方向萌生;在裂缝中,偏析成分形成球形夹杂物进入缝隙. 在尚未形成裂缝的区域,偏析聚集形成带状. 裂缝中

间含有球形和具有光滑表面的夹杂物,说明该裂纹 是由于偏析成分在高温下形成液膜,冷却过程中液 膜与两侧晶粒分离而导致的液化热裂纹.

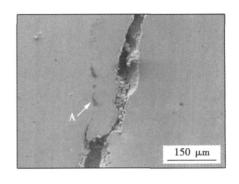


图 3 裂纹与偏析、夹杂物的关系 F g 3 Location of cracks and segregation & inclusion

成形件的主要组织是块状和条状先共析铁素体、针状铁素体、少量的珠光体和残余奥氏体.由于堆焊成形过程中相邻焊道的热影响作用,成形件的组织在局部范围内呈现一定的方向性.如图 4所示.由图 4可见,成形件中的裂纹主要存在于不同生长方向的晶界之间,沿晶界曲线延伸,遇到尺寸较大、生长方向一致的组织时发生偏转分叉,随着促进裂纹形成的能量不断耗散,裂纹最后终止.

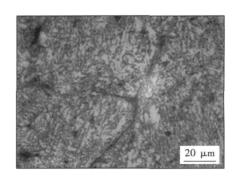


图 4 裂纹与偏析 Fg 4 Cracks and segregation

对图 3中偏析带上的 A点进行 EDS分析,如图 5所示. 由图 5可见, Ç Q Mṛ Si Mo和 N元素的含量均显著高于成形件的化学成分含量. 因此,偏析的主要成分应是 Mī和 S的氧化物、Mo的碳化物以及 N的金属间化合物. Mī和 S的氧化物在一定条件下会形成低熔点的锰硅酸盐,其熔点可低至1200 ℃左右<sup>[5]</sup>. 在多层多道焊的热循环过程中,如果部分锰硅酸盐来不及上浮到沉积层表面,残留在沉积层内部的锰硅酸盐在晶界上富集,形成低熔点的液态薄膜,最终在拉伸应力作用下导致结晶裂纹.

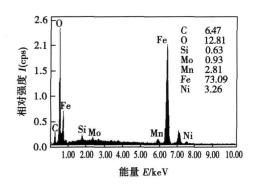


图 5 图 3中 A点的 EDS分析 Fig 5 EDS of spotA in Fig 3

对成形件中的  $\alpha$ 和  $\gamma$ 相含量分析表明, 成形件的残余奥氏体平均含量为 10.55%. 奥氏体可以显著降低有害元素  $\S$  P的溶解度, 造成有害元素的偏析. 同时, M0元素在奥氏体中的体扩散系数较小, 又是强碳化物形成元素, 其碳化物在奥氏体枝晶生长过程中容易偏析, 使碳化物大量弥散分布于奥氏体枝晶间, 造成材料基体组织和晶界间的浓度差别, 产生晶界脆化, 在拉应力作用下引起沿晶裂纹  $^{[6]}$ . 残余奥氏体的存在还导致成形件的导热系数低于低碳钢基板的导热系数, 而线膨胀系数大于低碳钢基板的线膨胀系数, 面线膨胀系数大于低碳钢基板的线膨胀系数, 固此, 在多层多道堆焊过程中容易在焊缝金属中形成较大的拉伸应力, 使得成形件的热裂敏感性显著增加.

综合以上分析,成形件中的裂纹形成机理为多层多道堆焊成形过程中,由于相邻焊道或下一沉积层对上一沉积层的热影响作用,偏析聚集在奥氏体晶界处的低熔点锰硅酸盐发生重熔,碳化物引起材料基体组织和晶界间产生浓度差,使焊缝金属产生脆性温度区,在拉伸应力的作用下,沿原奥氏体晶界开裂形成液化裂纹.液化裂纹一旦形成,在拉应力的持续作用下,沿着沉积层之间的晶界向下一层不断扩展,形成宏观裂纹.

### 3 影响裂纹形成的因素

#### 3.1 合金成分

堆焊成形材料合金体系的设计不仅要考虑单个元素对焊缝金属强韧性的作用,还要考虑与其它元素的协同作用. 从提高成形件强度和韧性的角度出发,提高了成形材料中  $M^n$ 和 N元素的含量. 事实表明,只有  $M^n$   $N^i$  S元素在最佳含量范围内才能有效地提高成形件的强韧性,并防止成形件产生热裂纹缺陷. 图 6所示为  $M^n$   $N^n$   $N^n$   $M^n$   $M^$ 

形缺口试样的冲击吸收功, $\sigma_y$ 为 y方向正应力. 由图 6可见,Mp N元素的含量过高时,将会导致焊缝金属热裂纹的形成.

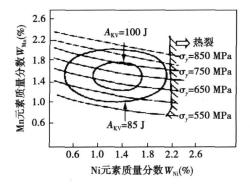


图 6 Mn和 N元素含量对焊缝金属热裂纹的影响 Fig 6 Effects of Mn and Nion hot cracks

#### 3 2 夹杂物

对裂纹中的夹杂物进行能谱分析, 结果如表 1 所示. 可见, 夹杂物与偏析的主要成分基本一致, 一方面验证了裂纹中夹杂物来源于偏析的推论, 另一方面也说明了裂纹的形成与 M<sup>--</sup>和 S的氧化物、M<sup>--</sup>的碳化物以及 N的金属间化合物有关.

表 1 夹杂物的能谱分析(质量分数, %) Table 1 EDS of inclusions

夹杂	С	О	Si	Mn	Mo	Ni	Fe
1	2 36	0. 81	0 30	_	0 62	2. 55	93. 36
2	2. 34	1. 50	0 49	1 90	0 68	2. 54	90. 54
3	2 08	0.60	0 40	_	3 65	_	93. 27
4	1. 26	0. 51	0 42	2 28	1 14	2. 74	91. 66

#### 3 3 应力分布

在堆焊快速成形过程中,焊缝金属会经历剧烈的温度变化. 当熔池金属凝固收缩时,由于受到周围凝固金属和基板的限制,不能自由收缩,导致焊缝金属中产生拉伸应力. 通过 ANSYS软件模拟单层沉积层中心点的应力一时间变化结果表明<sup>[7]</sup>,沉积层中焊缝金属承受的最大拉伸应力超过 250 MP<sup>2</sup>. 这个拉伸应力远大于存在残余液相的凝固金属的塑性和强度极限,直接导致凝固金属组织沿晶开裂,并且持续作用的拉应力促使裂纹沿沉积方向不断扩展. 因此,焊缝金属中的拉伸应力是形成裂纹的主要外因.

## 4 减少裂纹形成的措施

基于上述裂纹形成影响因素的分析,可以从三

个方面采取措施来减少或消除成形件中的裂纹. (1)适当降低奥氏体化元素 (如 Mṇ N元素)的含量,合理匹配 Mṇ Ni S元素的含量,避免这些元素带来的不利影响. (2)通过添加稀土元素 Cệ净化焊缝金属,使偏析球化,避免奥氏体晶界处形成液化薄膜. (3)采用层层正交的路径沉积,延长层间隔时间,降低层间隔温度,减少焊缝金属凝固过程中的应力累积,防止焊缝金属产生拉应力集中. 通过以上改进,对堆焊成形低碳钢件进行分析,均无裂纹产生.

### 5 结 论

堆焊成形件的裂纹萌生于初始沉积层,沿沉积高度方向扩展,终止于成形件表面之下,属沿晶液化热裂纹. 在多层多道堆焊成形过程中, Mn和 S的氧化物、Mn的碳化物以及含 N 金属间化合物的偏析是裂纹形成的内因, 焊缝金属凝固产生的拉应力是裂纹形成的外因. 通过合理匹配 Mn Ni S元素的含量,添加稀土元素 Cr改进成形材料,采用层层正交的路径沉积,延长层间隔时间,可以消除成形件的裂纹.

#### 参考文献:

[1] 李 超,朱 胜,沈灿铎 等. 焊接快速成形技术的研究现状与发展趋势[1]. 中国表面工程, 2009, 22(3), 7-12

- Li Chao, Zhu Sheng Shen Canduo, et al. Present state and development trend of welding rapid forming technology. J. China Surface Engineering 2009, 22(3), 7—12.
- [2] Zhang Yuming LiPengjiu Chen Yiwe, i et al. Automated system for welding based rapid prototyping J. Mechatronics 2002 12 37—53.
- [3] 陈 静、林 鑫、王 涛、等。316 L不锈钢激光快速成形过程中熔覆层的热裂机理[j]. 稀有金属材料与工程。2003—32(3): 183—186

  Chen Jing Lin Xin Wang Tao et al. The hot cracking mechanism of 316 L stainlness steel cladding in tapid laser forming process j. Rare Metal Materials and Engineering 2003—32(3): 183—186
- [4] 赵晓明,陈 静,何 飞,等,激光快速成形 Rene88DT高温 合金开裂机理研究[J]. 稀有金属材料与工程,2007。36(2). 216—220 Zhao Xiaom ing Chen Jing He Fei et al The cracking mechanism of rene88DT surperalpy by laser rapid forming J. Rare
- Metal Materials and Engineering 2007 36(2): 216—220.
  [5] 陈伯蠡、焊接冶金原理[M. 北京: 清华大学出版社, 1991
- [6] 钟定铭,刘建国,银锐明,等,堆焊金属裂纹形成机理研究 [J. 株洲工学院学报,2002 16(6): 87—89 Zhong Dinsming Liu Jianguo Yin Ruinin et al Study on the Principle of formation of heap soldering metal cracke J. Journal of Zhuhou Institute of Technology 2002 16(6): 87—89
- [7] 赵继勋. 基于机器人 GMAW 堆焊再制造成形层数值模拟研究 [1]. 北京: 装甲兵工程学院, 2008

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tents of alloying elements in the grain boundary were less than those in the base material and heat affected zone. The crystal cracks for welding in ZM6 magnesium alloy casting were found by observing the crack location and investigating the process of welding of ZM6 magnesium alloy casting

Key words. ZM6 magnesium allov casting TG repairing welling process method

Effect of pulse current frequency on microstructure and mechanical properties of 2219 alum num alloy weld joints CONG Backians QI Bojin LIW ei YANG Mingauan (School of Mechanical Engineering and Automation Beihang University Beijing 100191 China). P 37—40

Abstract The influence of pulse square wave current fre. quency on the microstructure and mechanical properties of 2219 hgh strength aluminum alloy weld joints was investigated based on a novel ultrafast convert hybrid pulse current variable polarity gas tungsten arc welding technique. The experimental results showed that comparing with no effect of pulse current the coarse grains changed to fine equiaxed grains A kind of finer equiaxed non den trites was observed distributing in the form of banding at the weld zone while the pulse current frequency was more than 20 kHz Mechanical properties of weld joints were improved predominantly at the given pulse frequency of 60 kH,z tensile strength and percentage elongation of weld joints are increased by about 17. 6% and 66%, respectively compared to that of weld joints with no effect of pulse current. At the given pulse current amplitude and pulse duty cycle with the pulse current frequency in certain range increased thewidth of fusion zone obvious ly decreased and the ductility of welds was improved significantly However, the variation in tensile strength of weld joints was relatively less sensitive with the increase of pulse current frequency

Key words high strength aluminum alloy high frequency pulse current pulse frequency equiaxed non-dentrite mechanical property

Form a tion characteristics of Ni/Ti in term etallics through annealing of layered Ni/Ti ZHOU Yong 2, YANG Guan Juri, WU Xiari, LI Changjiul (1. State Key Laboratory for Mechanical Behavior of Materials School of Materials Science and Engineering Xian Jiaotong University Xian 710049 China 2 School of Materials Science and Engineering Xian Shiyou University Xian 710065 China). P41—44

Abstract Ni/Ti diffusion couples were prepared by cold spraying with Ni and Ti powders and mechanically alloyed Ni/Ti alloy powders. The formation and growth characteristics of Ni/Ti intermetallics with in Ni/Ti during solid state diffusion treatment were investigated by scanning electron microscopy (SEM) and X-ray diffraction (XRD). It was found that the thicknesses of Ni/Ti NiTi and Ti/Ni intermetallic compounds layers increased with annealing temperature. The growth of TNi layer followed the parabolic law with annealing time while the thicknesses of Ti/Ni or Ni/Ti layers were kept constant at certain annealing temperature. The results suggest that the formation and then rapid growth of TNi intermetallic take place after Ni/Ti and Ti/Ni intermetallic compounds grow to certain thicknesses.

 $\begin{tabular}{ll} Keywords & Ni/Ti diffusion couples solid state diffusion annealing treatment in termetallic compound \end{tabular}$ 

Study of digital push-pull CO<sub>2</sub> welding system IU Zhenyang YAN Sibo YANG Shuai LIU Jia (College of Mechanical Engineering & Applied Elections Technology Beijing University of Technology Beijing 100124 China), P45—48 52

Abstract. The digital Push & Pull CO<sub>2</sub> welding system is proposed. This system utilize digital power source controlled by DSP and CPID as platform with the AC servo push pull feeder with the low moment of inertial fast response and steady feed speed. The constant feeding part combine with push pull feeding part to form the whole feeder using buffer as a linker. Consider the characteristics of the push pull short circuit CO<sub>2</sub> welding technics the feeder speed curve welding voltage and current waveform control program was predesigned. According to soft ware program, the steady push pull CO<sub>2</sub> welding technics was a chieved with low spatter, low heat input and uniform dioplet.

K ey words d'gital power source push pull feeder  $CO_2$  we heat input

Study on structures and properties of Part made by microplasma are direct metal formation. XANG Yonghuat?, XUB inship IV Yaohui (1 Navy Logistic Technology and Equipment Institute of PLA Beijing 100072 China, 2 National Key Laboratory for Remanufacturing Academy of Armored Forces Engineering Beijing 100072 China). P49—52

Abstract The deposition experiments were done on the mild steel by micro plasma are powder overlaying rapid prototy. Ping technique with Fe313 alloy powder. Them icrostructures and morphologies were observed by metallographic microscope and SEM, the microhardness was tested by vickers. It was showed that the middle layer displayed insular M.-A component structure and the interface between layers was evident. The microstructure of Fe based deposited layer was affected by the subsequent over laying with annealing process, and the crystalline grain refined. The hardness distribution curve of the cylindraceous part was as U shape, the middle layer was soften because the drawing effect of subsequent layers.

Key words rapid prototyping microplasma arc overla ying Febased alby microstructure

Cracking formation mechanism of mild steel parts fabricated by surfacing rapid forming LI Chao, LIANG Yuanyuan SHEN Canduo, ZHU Sheng (National Defence Key Laboratory for Remanufacturing Academy of Armored Forces Engineering Beijing 100072 China). P53—56

Abstract. The micro morphology of cracks for the parts fabricated by surfacing rapid forming was observed with SEM. The results showed that the cracks initiated from the first layer of the part, extended along the deposition direction, and finally terminated under the surface of the part. The segregation and inclusion in the formed partwere studied by OM and EDS moreover, the content of residual austenite was measured by XRD. The results indicated that the cracks were lituid hot cracks. In course of forming with multi-layers and multi-paths, the segregation comprised of Mn and Si oxidate. Mo carbide and Ni intermetallic compound were the internal cause for the cracks formation, while the tension stress was the external cause. By properly matching the contents of Mn, Ni and Si elements, purifying the well metal with rear earth elements cerium, adopting the orthogonal depositions.

tion paths layer by layer and prolonging the interformational intervals the cracks could be avoided

Key words  $% \left( \frac{1}{2}\right) =0$  surfacing rapid forming metal cored wires  $crad_{k}$  segregation

Effect of loading rate on shear strength of SnA &Cu solder joint IUW ei ZHANG Ning SHI Yaowu LEI Yongping (School of Materials Science and Engineering Beijing University of Technology Beijing 100124 China). P57—60

Abstract Effect of bading rate on shear strength and fracture mode of SnAgCu (SAC) lead-free solder joint was investigated. The Ag content of the solders used in the experiment was 1% to 3%. The loading rate of the solder joint was 0.01 mm/s to 10 mm/s. The results indicated that the shear strength in creased with the increase of bading rate and fracture with ductile feature occured inside the solder, when the bading rate was less than 1 mm/s. When loading rate reached to 10 mm/s, the shear strength decreased and brittle fracture occured in the intermetallic compounds layer of pint Moreover, shear strength increased with Ag content of solder increased at low loading rate, while the shear strength of solder pint with 2% Ag was the lowest at high loading rate

Keywords lead-free solder loading rate shear strength

Effect of vanadium on property of FeCrC hardfacing a loy WANG Zhihui HE Dingyong YU Changli JIANG Jian min (College of Materials Science and Engineering Beijing University of Technology Beijing 100124 China). P61—64

Vanadium was added to Fe.Cr.C hard facing alloy and its effect on the property of the alloywhen welded and reheated was studied. The hardfacing layers were produced on Q235 mild steel by sulmerged are welding method. The micro. structures wom surface of the overlayer were examined by means of optical microscope and scanning electron microscopy (SEM). Abras ive wear resistance and hardness were tested The results showd that heating process had effect on the hardness of the alloy. The hardness of matrix decreased more than 22% by rehea. ting The max hardness decreased 37 7/10 with no vanadium. But it has little effect on the hardness of primary carbide of which the hardness decreased on 1/2, 4% -11, 3% by reheating Vana dim could increase the abrasion property of post heated FeCrC hard facing alloy. Using the loss weight of quenched 45 sample as abrasion test bench mark the lative abrasion value of the alloy content of 0.4% vanadium was 1.9 In the same condition, that of the allow with no vanadium contentwas on 1/1 3. The abrasion property increased 46%.

Keywords FeCrC hard facing allow, vanadium element post heat treatment carbide abras on wear

Simulation of temperature field and residual stress field of thin inner layer on butt welling of clad pipe. YU Jian rong, HE Xiaoxians<sup>2</sup>, WU Bo, CHEN Haiyang, LI Xiaodong (1 School of Mechanical Engineering Beijing Institute of Petrochemical Technology Beijing 102617 China 2 College of Mechanical and Electrical Engineering Beijing University of Chemical Technology Beijing 100029 China). P65—68

Abstract The clad pipe has a thin inner layermade of stainless steel and a thick outer layermade of cathon steel and the outer layer has some restriction on the temperature change

surrounding the inner layer when buttwelling the inner layer. With finite element method the temperature field was computed when buttwelling inner layer and the stress field of inner layer was computed after buttwelding. The convection radiation and contact effect between the wo layers were considered in the FEM model as well as temperature depended material properties. In temal heat generation loading method was applied to simulate heat source and model change ability to simulate buttweld. The velocity of inner layer buttweld the temperature and stress field of the inner layer were discussed. Meanwhile the influence of the properties of material geometry of the plate and the welding heat input on buckling distortion were analyzed based on the simulations. The results indicate that the geometry of the plate and the welding heat input have more effect on distortion than the properties of material.

Keywords clad pipe buttweld finite element analysis stress field contact effect

M icrostructure characteristic and perform ance of bonding interface between than immalpy/copper/GCr15 LIU Shuying, ZHANG Guifeng, LU Guangbad, XU Peilf, WANG Yawel (1. Henan Province Key Laboratory of Advanced Nonferrous Metals School of Materials Science and Engineering Henan University of Science and Technology Luoyang 471003 Henan China 2 Welling Research Institute Xian Jaoong University Xian 710049 China 3 Department of Electrical and Electronic Henan Technician College of Economics and Business Xinxiang 453700 Henan China 4 Shanghai Heavy Machinery Plant Limited Corporation, Shanghai 200245 China). P69—72 76

Difficulty for diffusion bonding of different Abstrac<u>t</u> structure of titanjum alloy/bearing steel testricts the application of titanium alby. The mechanical properties of  $T_{i6}A_{l4}V/C_{u/l}$ GC 1/5 joints were evaluated by electronic tensile machine. The m icrostructure characteristic and performance of the bonding in terface were analyzed by scanning electron microscopy and EDX Microhardness the fracture characteristics and area of interme. tallic compounds of the joints were analyzed by  $X_-$  ray diffraction The results indicated that the tensile strength of the pints under the bonding time 1. 8 k,s pressure 4 9 MPa rises with the bonding temperature the tensile strength of joint reaches amaxi mum of 206 MPa in 1 273 K. The extension bonding time caused the intermetallic compound thickness to increase which would do harm to the pints performance  $\alpha$ -Ti(Cu) solid solution which was generated in bonding interface was advantageous to enhance the joints performance. However, the Ti<sub>x</sub>Cu<sub>y</sub> had more influence on pints performance which was Ti Cu Ti Cu (Ti Cu) FeTi those caused the joint strength to go down. Copper foil should not be too thick to be as interlayer in titanium/GCn5

Key words interlayer diffusion bonding banding interface tensile strength intermetallic compounds

Heat source modeling and power density analysis for vacuum electron beam welding LUO Y 12, XU Huibir, LI Chuntiari, WU Guangfeng (1. School of Material Science and Engineering Chongqing University of Technology, Chongqing 400050 China, 2 School of Material Science and Engineering Northwestern Polytechnical University, Xian 710072 China). P 73—76