Vol. 28 No. 12

December 2007

铜 网 TIG 堆焊氦一氩混合比对泛铁的影响

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摘 要:研究了不同氦一氩混合比在铜/钢 TIG 堆焊过程中对泛铁量及泛铁形态的影响。通过调解氦一氩混合比来获取相应的电弧形态及电弧压力,得到了不同氦一氩混合比与泛铁量及泛铁形态之间的关系。结果表明,在适当的焊接工艺参数下,随着氦气比例的增加,热输入增大,而电弧压力先减小后增大。不同的氦一氩混合比对应不同的泛铁形态。通过调节氦一氩混合比来实现对电弧的热输入、电弧压力及电弧形态的控制,从而严格控制泛铁量及泛铁形态。

关键词: 氦-氩混合比; 电弧形态; 电弧压力; 泛铁量及形态 中图分类号: TG115.28 文献标识码: A 文章编号: 0253-360X(2007)12-101-05



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0 序 言

航空航天领域,为了改善钢材的导电、导热性能和表面硬度,通常需要在钢基体表面堆敷铜合金层。在兵器制造业领域,钢表面堆敷铜合金技术也有广泛的应用,例如炮弹弹带即是在钢基体上堆焊铜合金层。铜/钢堆焊过程中,铜合金与钢的界面化学成分急剧变化,在界面处将会发生钢基体向熔融的铜的扩散和溶解,该扩散和溶解量称为泛铁量,该数值的大小将会影响到铜/钢复合接头的强度和硬度。因此,考虑泛铁量在TIC 堆焊过程中的影响因素对铜/钢复合接头的质量以及实际焊接工艺的制定都具有一定的指导意义。

Cu 和 Fe 在液相无限互溶,所以相互扩散的结果使得熔合区中 Cu 和 Fe 为缓变特征。在固态,Cu 和 Fe 有限固溶,以富 Cu(ε)+富 Fe(α)相的双向固溶体组织存在 在铜 钢 TIG 堆焊过程中,电弧的热输入、电弧压力及电弧形态是决定泛铁量及泛铁形态的重要因素。由于电弧形态及电弧压力的作用,熔池表面发生严重的变形,随着电弧形态的变化及电弧压力的增大,熔深增大,熔池表面最大下凹和凸起亦增大,钢基体的熔化量增加,钢基体向熔融的Cu 的扩散和溶解的行为增强,泛铁量亦增大。采用氦一氩混合比能有效控制热输入、电弧压力及电弧形态。

1 试 验

1.1 电弧压力及形态试验装置

通过改变氦气和氩气的混合比例,来测定不同氦一氩混合气体下的 TIG 电弧形态及电弧压力。采用通用的静态小孔法^[2],设备装置如图 1 所示。对燃烧稳定的不同氦一氩混合比下的 TIG 堆焊电弧压力分布进行测量,在阳极水冷铜板开 0.3 mm 的测量小孔,将其作用于该点的电弧压力通过压力导管传至压差传感器。把压力值转换为电信号。最后,再由计算机还原为压力值。调节氦一氩混合比例。测量当前电弧压力值,通过电弧形态演示器观察电弧形态,再将待测试件放在水冷铜板位置,电弧对准待测试件上的测量小孔,待电弧稳定后,由计算机读取电弧压力值。

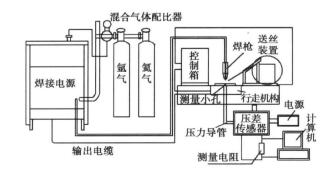


图 1 氦一氩混合气体电弧压力测量系统
Fig 1 Schematic diagram of arc pressure measurement system under Ar— He mixture gas

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1.2 试验材料及方法

母材及堆焊焊丝成分分别如表 1 和表 2 所示。 采用 TIG 焊接方法进行堆焊试验。焊接电弧的热输 入可分为两部分,一部分为焊丝熔化热,作用于堆焊 焊丝上,另一部分则直接作用于基体上,用于熔化母 材。

表 1 基体母材成分(质量分数, %)
Table 1 Chemical composi of base metal

С	Mn	Si	P	
~ 0. 22	$0.3 \sim 0.65$	< 0.3	< 0.05	

表 2 堆焊焊丝成分(质量分数, %) Table 2 Chemical composi of filler metal

Cu	Al	Si	Mn	Pb	Sn	P	其余杂质
≥98.0	≪0.01	≪ 0.5	≪0.5	≤0.02	≤1.0	≪0.15	≤0.50

2 氦--氩混合比电弧形态及压力分析

2.1 不同氦一氩混合比的电弧形态

氫气密度比空气的大,而比热容和热导率比空气的小,这些特性使氫气具有良好的保护作用和稳弧作用。与氫气相比,氦气电离电位高,热导率大[□],在相同的焊接电流和电弧长度条件下,氦弧的电弧压力比氩弧的低,电弧有较大的功率。并且氦气冷却效果好,使得电弧能量密度大,弧柱宽,焊缝有较大的熔宽及熔透率。不同氦一氩混合比下的电弧形态如图 2 所示,电弧高度为 5 mm,随着氦气含量的增加,电弧宽度逐渐变宽,焊缝的铺展行为增强,焊缝宽度宽,泛铁量增大。

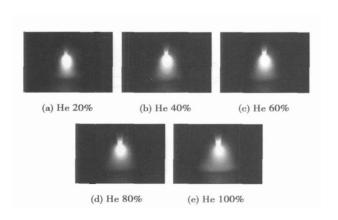


图 2 不同氦一氩混合比的电弧形态

Fig. 2 Arc appearance of different poropertion of Ar— He mixture gas

2.2 不同氦一氩混合比的电弧压力

电弧压力主要是由电弧静压力和电弧动压力组成,电弧静压力是由电磁收缩效应引起的,电弧动压力是由电弧中粒子对工件的撞击引起的¹⁹。其中,电弧静压力不但直接作用于熔池表面,而且是电弧动压力的力源。

与氫气相比, 氦气电离电位高, 热导率大, 增加 氦气混合比能有效地增大热输入, 而电弧压力在氦气增加的同时先降低, 当氦气混合比例达到 85%以上时, 电弧压力呈升高趋势, 如图 3 所示电流为270 A, 不同电弧高度及氦一氩混合比对应的电弧压力分布情况。

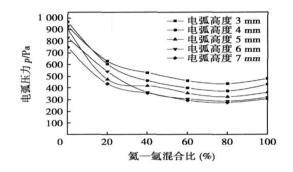


图 3 不同氦一氩混合比的电弧压力分布 Fig. 3 Arc pressure distribution in different He—Ar gas ratio

在纯氩气氛,要得到与氦一氩同等的热输入,只有增大焊接电流,增大焊接电流的同时,电弧压力急剧升高,电弧的搅拌作用增强。图 4 为相同热输入下不同氦一氩混合比的电弧压力分布规律,从图 4 中可以看出,相同的热输入,纯氩的电弧压力最高,随着氦气比例的增加,电弧压力逐渐下降,当氦气比例增加到80%以上时,电弧压力回升。

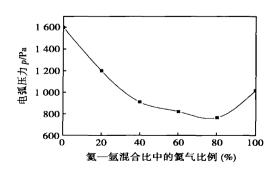


图 4 相同热输入不同氦—氩混合比的电弧压力

Fig 4 Arc pressure with different He—Ar gas ratio in similar heat input

3 不同氦—氩混合比对泛铁的影响

3.1 不同氦一氩混合比对泛铁量的影响

堆焊过程中, TIG 电弧除了作为热源外, 其另一个主要作用是作为压力源。当电流较小时, 基体未熔化, TIG 电弧压力作用在熔融态的铜合金上成为促进铜合金在基体上铺展的驱动力; 当电流加大到使基体熔化时, TIG 电弧压力成为了促进液态 Cu 与液态基体双相对流的驱动力, 在电弧压力的搅拌作用下, 液态 Cu 与液态钢基体除了发生溶解与扩散外, 还发生机械混合, 这极大地增加了铜合金层中Fe 含量, 同时也改变了Fe 元素的分布。在如表 3 所示的焊接工艺参数下, 通过调节氦一氩混合比来达到调节电弧形态、热输入及电弧压力的目的。

表 3 焊接工艺参数 Table 3 Welding parameters

	送丝速度	焊接电流	电弧高度
$v_{\rm w}/({\rm mm \cdot min}^{-1})$	$v_{\rm g}/({\rm mm} \cdot {\rm min}^{-1})$	$I/\!\mathrm{A}$	$h/_{\!\!\mathrm{mm}}$
190	3 000	270	5

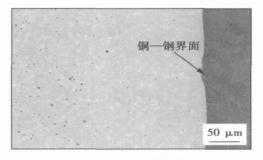
增加氫一氦混合比中氦气的含量,热输入明显增大,而电弧压力降低,电弧搅拌能力降低,电弧的挖掘能力降低。在基体微熔过程中,界面随着氦气比例的增加而变得平直,机械混合层厚度增加,泛铁量呈缓变增加趋势,如图 5 所示。当氦气增加到80%以上,基体大量熔化,热输入和电弧压力都增大,泛铁量急剧升高,如图 5d 所示。

3.2 不同氦一氩混合比对泛铁形态的影响

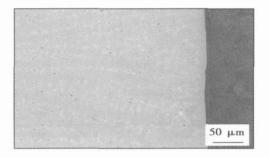
焊接熔池中的传热过程, 电弧的搅拌作用, 决定着堆敷层金属的晶体成长形态, 决定着 Fe - Cu 液相分离现象的发生以及 Fe 在堆敷层中的泛铁分布形态^[5.6]。

在表 3 所示的焊接工艺参数下, 氦气的比例在 50%以下时, 铁基体微熔, 在氦气比例较小时, 电弧压力大, 电弧的搅拌作用强, Fe 的密度比 Cu 低, 在固相有限互溶, 如图 6a 所示在氦气含量为 40%时, Fe 在液态 Cu 中上浮, 电弧压力及电弧搅拌作用较弱, 铁基体在扩散过程中的表面自由能逐渐降低, 结晶后易形成类球状泛铁形态, 析出的富 Cu(ϵ)+富 Fe (α)相的双相固溶体。其固溶体成分如图 6b 所示。

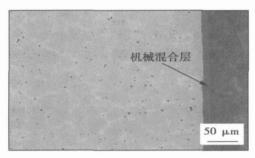
氦气的比例逐渐增加到 70%以上时,出现大量泛铁,热输入增大,钢基体熔化量增加,液态Cu和



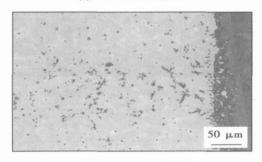
(a) He 20% 的泛铁量



(b) He 40% 的泛铁量



(c) He 60% 的泛铁量



(d) He 80% 的泛铁量

图 5 不同氦--- 氯混合比的泛铁量

Fig 5 Shape Fe solid solution at different He Ar gas ratio

Fe 在液相无限互溶, 电弧压力呈下降趋势, 泛铁在液态 Cu 中流动性好, 如图 Ta 所示, 类球状的富 Cu (ε)+富 $Fe(\alpha)$ 相的双相固溶体有足够的生长平台, 在 Te 元素向 Cu 的扩散过程中, Te 元素的流动性增强, 在 Te 元素上浮过程中, 易于生长成类枝状泛铁形态。类枝状泛铁的成分如图 Te 所示。

氦气的比例逐渐增加到85%以上时,由于热输入的进一步增大,熔深及熔宽增大,电弧压力也随着

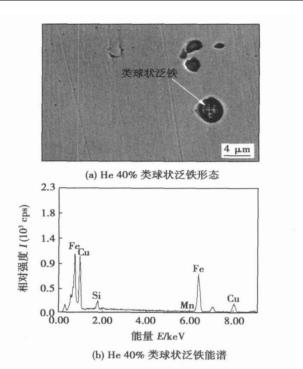
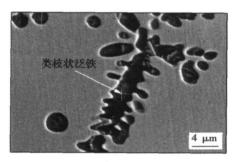


图 6 类球状泛铁形态及能谱

Fig. 6 Morphology and EDS spectrum of quasi-spherical Fe solid solution



(a) He 80% 类枝状泛铁形态

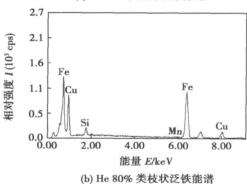
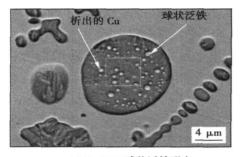


图 7 类枝状泛铁形态及能谱

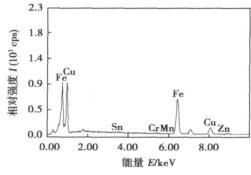
Fig. 7 Morphology and EDS spectrum of quasi-dendrite Fe solid solution

氦气的增加呈上升趋势,大的电弧压力作用下,液态 Fe 在液态 Cu 中上浮的过程中,电弧搅拌作用增强,

使得泛铁的表面张力减小, 易于以表面张力小的球状泛铁形态析出。 Cu 在球状泛铁中的析出情况如图 8a 所示, 其成分如图 8b 所示。



(a) He 90% 球状泛铁形态



(b) He 90% 球状泛铁能谱

图 8 球状泛铁形态及能谱

Fig 8 Morphology and EDS spectrum of spherical Fe solid solution

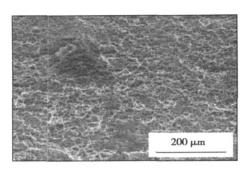
4 结 论

- (1) 改变 氦一氫混合比能有效地控制电弧压力、电弧形态及热输入,从而有效地控制泛铁量。
- (2) 氦一氩混合中的氦气比例不超过 80%时, 基体微熔,泛铁量呈缓变增加趋势,当超过 80%,电 弧的热输入及电弧压力都增大,泛铁量由缓变增加 趋势变成急剧增加趋势。
- (3) 通过改变氦—氩混合比能够有效地调节泛 铁形态。

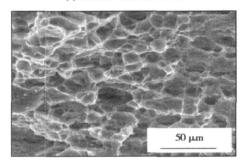
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(a) 拉伸断口低倍放大形貌



(b) 拉伸断口高倍放大形貌

图 4 铝合金拉伸试样断口扫描形貌
Fig. 4 SEM fractography of aluminum alloy tensile specimen

5 结 论

(1) 双光点激光焊接在两光点间距较小,未完

全分离时,热源作用与单激光焊接相似,但散热方向更为复杂,晶粒生长接近焊缝中心时方向改变更明显,晶粒的生长受到限制,组织得以细化。

- (2) 5052 铝合金的单激光焊接与双光点激光焊接的焊缝及热影响区硬度均高于母材, 双光点激光焊接接头硬度低于单激光焊接接头, 有利于接头脆化的改善。
- (3) 双光点激光焊接接头抗拉强度高于单激光焊接接头与母材, 断后伸长率相差不大。
- (4) 室温拉伸断裂在母材处发生,是比较典型的韧度断裂过程,断口为韧窝形貌。

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Abstract: The influence of boron and chromium on wettability of nickel-based high temperature filler metals on carbon fiber reinforced silicon carbide composite (3D— C_f \dot{S} iC) was studied. It was found that at 1 200 $^{\circ}$ C for 10 min under vacuum when the content (wt, %) of chromium equals to 15% and boron equals to 0.6%, the contact angle of nickel based filler metal on C_f/\dot{S} iC is 10 degree. While, as the content of boron adds to 2.4%, the angle increases to 62 degree. It indicates the boron reduces the wettability. The experiment results indicates the element chromium can promote wettability greatly. The wetting procedure is reactive wetting, and several carbides and silicides were formed at interface.

Key words: nickel-based high temperature filler metal; wet tability; $C_{\rm f}/{\rm SiC}$

Intergranular fracture of weld metal of structure steel in a ship structure at lower temperature and higher loading rate LIU Ruitang FENG Wanli, CHEN Fengqiu, GUO Chunhuan (College of Materials Science and Chemical Engineering, Harbin Engineering University, Harbin 150001, China). 97—100

Abstract: Effect of lower temperature and high loading rate on the fracture behaviors of weld metal was studied. The results indicated that the fracture toughness reduces and the tendency to intergranular fracture increases with both reducing temperature and raising loading rate, which shows the low temperature effect and high loading rate effect and both of them promot each other. Intergranular fracture results from the inter action of metallurgical structural and environmental factors. The tendency to intergranular fracture depended on the ability of grain boundary to suit with plastic deformation of adjacent grains. The intergranular brittle fracture will occur if the grain boundary can not suit with the plastic deformation.

Key words: intergranular fracture; high loading rate; low temperature; weld metal

Effect of mixed He— Ar gas ratio on Fe content in TIG surfacing LV Shixions, YANG Shiqin, YANG Tao (State Key Laboratory of Advanced Welding Production Technology, Harbin 150001, China). p101—104, 108

Abstract: The effect of the mixed He—Ar gas ratio on the quantity and morphology of Fe content in TIG surfacing of copper-steel was studied and the relationship was obtained by adjusting the He—Ar gas ratio which can affect the according arc morphology and arc pressure. The results show that the amount of heat input increase with the increase of He content in appropriate welding parameters while the arc pressure decrease first and increase later. Moreover,

the morphology of Fe content is different in different He—Ar gas ratio. In addition, the amount of heat input, are morphology and are pressure can be controlled by adjusting the He—Ar gas ratio. Consequently, the quantity and morphology of steel can be controlled strictly.

Key words: He— Ar gas ratio; arc morphology; arc pressure; quantity and morphology of Fe content

Microstructure and mechanical properties of twin spot laser welding of 5052 aluminum LI Qiaoyan¹, LUO Yu¹, WANG Yajun², CHEN Li²(1. School of Materials Science and Engineering Dalian Jiaotong University, Dalian 116028, Liaoning, China; 2. Beijing Aeronautical Manufacturing Technology Research Institute, Beijing 100024, China).p105—108

Abstract The twin spot laser welding could significantly improve weld quality. For aluminum, surface quality was improved with fewer surface defects such as undercut, surface roughness spatter, and underfill. The microstructure of twin spots laser welding joint of 5052 aluminum alloy with 2. 0 mm thickness was observed. The mechanical properties, such as the microhardness and the tensile properties at room temperature were also tested, meanwhile the fractography was observed. It is shown that the structure of twin spot laser welding is finer and the microhardness is higher than the ones of the base metal, but lower than single laser welding is higher than that of single laser welded joint and the base metal.

Key words: aluminum; twin spot; laser welding; structure; mechanical properties

Analysis of stress concentration in weld of sheets welded by friction stir welding using finite element method YANG Fengping, SUN Qin (School of Aeronautics Northwestern Polytechnical University, Xi an 710072, China). p109—112

Abstract In order to study the tensile stress state of an aluminum alloy sheet welded by friction stir welding in airplane, three models of welded sheets which were distinguished by weld geometrical type of plane, protrude, concave were built in ANSYS' preprocessor. In each model, a symmetrical constraint condition was acted on the left end surface while a tensile stress was loaded on the right. A numerical simulation result was obtained with such conditions after ANSYS' solution. The result shows that the stress concentration of the welds depend on their geometrical shapes. If the model is concave or protrude, the eccentric bending caused by the tensile stress will affect the distribution of the stress. Especially if the model is concave the eccentric bending will make the stress concentration shap in the weld area and the deflection obvious in the end surface of the sheet.

Key words: friction stir welding; stress concentration; eccentric bending; finite element method