

氢对自保护药芯焊丝焊缝金属韧度的影响

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**摘 要:** 通过刻槽锤断试验、低温冲击韧度试验和扫描电镜分析等试验手段, 研究了焊后室温条件下, 放置不同时间的自保护药芯焊丝焊缝金属中氢含量对低温韧度的影响。结果表明, 由于自保护药芯焊丝中氢含量较多而脱氢能力不足, 并且熔池的存在时间相对较短, 焊缝金属中的氢不能充分逸出, 使得焊缝金属中含氢量较高(焊后立即进行试验); 在氢和非金属夹杂物的共同影响下, 低温冲击吸收功的平均数值较低, 而且数据的离散度大; 室温放置 40 d 以后, 焊缝金属中的氢含量减少, 刻槽锤断试样表面的氢白点减少或消失, 低温冲击吸收功的平均值提高, 数据的离散度降低。

**关键词:** 自保护药芯焊丝; 长输管道; 氢白点; 冲击吸收功

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0 序 言

随着世界能源需求的日益增长, 国内外输油输气管道建设逐渐趋向于高压、高钢级的方向发展, 这对于焊缝金属的强度和韧度提出了更高的要求。目前, 长输管道焊接施工中普遍采用的焊接方法是自保护药芯焊丝半自动下向焊。它具有高效、节能、综合成本低、环境适应能力强、熔敷金属成分调整方便等特点, 相对于焊条和实心焊丝而言更适合于长输管道高钢级的发展方向。然而, 自保护药芯焊丝半自动焊存在着两个突出的问题, 即焊缝金属刻槽锤断试样(拉断或弯断)表面常常有氢白点(鱼眼); 以及焊缝金属低温冲击吸收功的数据不稳定。

自保护药芯焊丝熔敷金属的氢含量是比较低的。由于药芯具有一定的含水量, 特别是焊丝的表面需要涂一层润滑剂来防锈和保证送丝顺畅, 因此其焊缝金属的扩散氢含量不可能控制得很低, 一般为不大于 8 mL/100 g, 这远远高于低氢型焊条和实心焊丝的扩散氢含量。另外, 自保护药芯焊丝在药芯中加入氟化物及铝、镁等易蒸发和脱氧固氮的物

质, 在焊丝熔化时能产生大量气体, 再加之熔渣的保护作用, 从而防止了空气中氮侵入电弧区及熔池, 降低了焊缝金属气孔敏感性。但是大量残留的脱氧剂则以 AlN, Al<sub>2</sub>O<sub>3</sub> 等夹杂物的形式存在于焊缝金属中。这些微观缺欠在焊缝金属承受拉伸应力时就成为焊缝金属中残余氢的聚集地, 是使低温冲击吸收功数值下降的区域。文中主要研究自保护药芯焊丝焊缝金属中的氢含量对低温韧度的影响规律。

1 试验材料及方法

母材为 API spec 5L X65 钢管, 规格 Φ914 mm×14. 68 mm。焊接材料为 AWS A5. 29 E71T8 自保护药芯焊丝, 规格为 Φ2. 0 mm。熔敷金属扩散氢含量为 6. 8 mL/100 g。母材和焊接材料熔敷金属化学成分如表 1 所示。焊接设备是具有平外特性的直流焊接电源及其相匹配的送丝机。焊接参数: 焊接电流 240 A, 电弧电压 19 V, 送丝速度 2. 29 m/min, 焊丝伸出长度 20 mm, 焊接极性为直流正接(焊丝接负)。

表 1 X65 钢管和 E71T8 自保护药芯焊丝熔敷金属化学成分(质量分数, %)  
Table 1 Chemical composition of X65 pipe and self-shielded flux-cored welding wire E71T8

材料	C	Si	Mn	P	S	V	Cr	Al	Ni	Mo	Cu	Nb	Ti	Fe
X65	0. 05	0. 29	1. 26	0. 005	0. 001	0. 014	0. 03	0. 023	0. 15	0. 00	0. 29	0. 049	0. 000 1	余量
E71T8	0. 041	0. 042	0. 867	0. 011	0. 006	0. 003	0. 024	0. 791	1. 018	0. 027	0. 015	0. 007	0. 003 0	余量

试件焊接后,分为两组。其中第 1 组立即制取试样进行刻槽锤断试验和低温冲击韧度试验,第 2 组则在环境温度下放置 40 d 后再制取试样进行刻槽锤断试验和低温冲击韧度试验。并且分别对这两组试件的典型低温冲击试样进行断口形貌的扫描电镜分析。

刻槽锤断试验按照 API 1104 标准在 WAW—600 拉伸试验机上进行。低温冲击韧度试验按照 ASTM A370 标准在 JB—500B 冲击试验机上进行,试样尺寸为 55 mm×10 mm×10 mm, V 型缺口开在焊缝金属上,试验温度为−20 ℃。低温冲击试样断口形貌扫描电镜分析采用 JSM6360LV 扫描电镜。

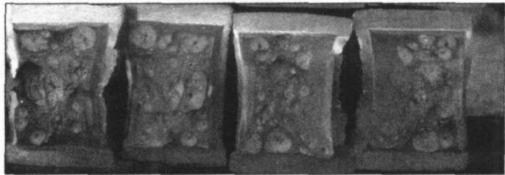
## 2 试验结果

### 2.1 刻槽锤断试验结果

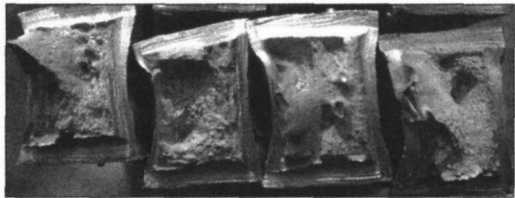
两组试样刻槽锤断断口照片见图 1。从图中可以看出,第 1 组试样的断口表面分布着大面积的氢白点,氢白点中心的夹杂物清晰可见。第 2 组试样断口表面的氢白点明显减少,甚至消失。

### 2.2 低温冲击韧度试验结果

两组试样的低温冲击韧度试验结果如表 2 所



(a) 第 1 组试样



(b) 第 2 组试样

图 1 两组试样焊缝金属断口表面形貌

Fig 1 Surface fractograph of two group specimen

示。第 1 组试样低温冲击吸收功的平均数值较低,且数据的离散度较大。6 个试样中有三个试样的冲击吸收功较低。第 2 组试样低温冲击吸收功的平均值提高,数据的离散度降低。6 个试样中仅有一个试样的冲击吸收功比较低。

表 2 焊缝金属−20 ℃冲击试验结果  
Table 2 Result of Charpy impact test in −20 ℃

试样号	冲击吸收功 $A_{kv}/J$							
	单值 $A_{kv}/J$		平均值 $\bar{A}_{kv}/J$		单值 $A_{kv}/J$		平均值 $\bar{A}_{kv}/J$	
第 1 组试样	95	59	110	88.0	72	100	68	80.0
第 2 组试样	102	118	112	110.6	114	108	80	100.7

### 2.3 低温冲击试样典型断口扫描电镜分析

两组低温冲击试样典型断口形貌的扫描电镜照片见图 2 和图 3。图 2 为脆性断裂断面,以扇形花样的解理形貌为主,有少量撕裂棱,有不明显的韧窝形

貌(小而浅),偶见舌形花样与穿晶二次微裂纹。图 3 为韧性断裂断面,是典型的韧窝形貌,窝底球状物为氧化物,带棱角的为氮化物,韧窝较深。图 4 为焊缝金属中的复合氧化物夹杂物。

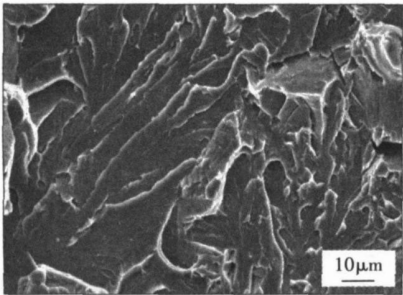


图 2 第 1 组的试样 2 断口形貌的扫描电镜照片  
Fig. 2 Fractograph by SEM of specimen No. 2(Group 1)

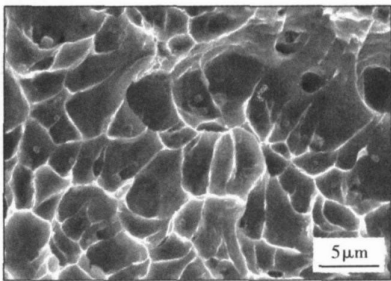


图 3 第 2 组的试样 2 断口形貌的扫描电镜照片  
Fig 3 Fractograph by SEM of specimen No. 2(Group 2)

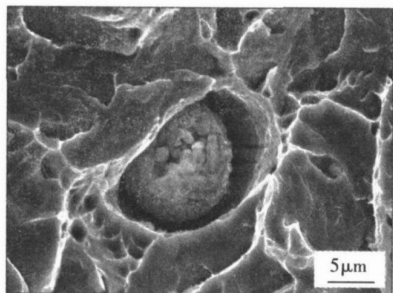


图 4 第 2 组的试样 6 焊缝金属中的复合氧化物夹杂物

Fig. 4 Compound oxide inclusion in weld metal of specimen No. 6 (Group 2)

## 3 讨 论

### 3.1 自保护药芯焊丝的焊缝金属含氢量

石油、天然气长输管道焊接工程中,常用的焊接材料的扩散氢含量分别为:纤维素型焊条 20~40 mL/100 g,低氢型焊条 3~5 mL/100 g,实心焊丝不大于 2 mL/100 g,自保护药芯焊丝 5.5~7.5 mL/100 g。由于自保护药芯焊丝含有较多的脱氧剂和脱氮剂,电弧气氛中氧化性较弱、还原性较强,所以氢含量多,而脱氢能力就显得不足。此外,由于 X65 母材中含有较多的吸氢元素 Nb 和 Ti,在熔池状态和随后的结晶过程中会吸收较多的氢。另外,自保护药芯焊丝半自动焊的焊接速度相对较快,熔池尺寸相对较大,而熔池存在的时间相对较短。因此,焊接焊缝金属结晶时有相当多的氢来不及逸出而被封闭在固态焊缝金属中。所以,采用自保护药芯焊丝焊接所得到的焊缝金属中的含氢量相对较高。

### 3.2 焊缝金属冲击吸收功的影响因素

文献[1,2]通过研究两种含铝量不同的自保护药芯焊丝焊缝,分别代表自保护药芯焊丝熔敷金属中铝含量的极限(1.7%和0.53%),预测其微观组织结构变化。文献[1]认为,在高铝焊缝金属中,AlN的形成优于 $Al_2O_3$ 和Ti(C,N)的形成,在低铝焊缝中则相反。文献[2]认为,高铝焊缝的微观组织结构呈现出典型的骨架状铁素体晶粒,低铝焊缝中呈现出典型的 $\alpha$ -铁素体柱状晶粒,低铝焊缝的微观组织好,具有良好的力学性能。文献[3]认为,AlN和 $Al_2O_3$ 都属于变形率低的脆性夹杂物,由于夹杂物与焊缝之间变形能力的显著差异,势必造成夹杂物与焊缝交界处产生应力集中,导致产生微裂纹或使夹杂物本身开裂,从而使焊缝金属的冲击吸收功降低。图4所示为氧化物的夹杂,当焊缝金属含氢量较高时,氢在夹杂物和其它微观缺陷边缘的空隙聚集,结

合为氢分子,使空腔内产生很高的压力,促使夹杂物边界产生微裂纹或夹杂物本身开裂。当V形缺口的位置恰好位于夹杂物附近时,就会造成低温冲击吸收功的突然下降。当焊缝金属中的含氢量降低以后,氢对夹杂物的启裂影响消失,使得低温冲击韧度得到改善,冲击吸收功数据的离散度降低。

### 3.3 氢的逸出及对焊缝金属性能的影响

由于冷却速度过快而封闭在焊缝金属中的氢处于过饱和状态,要极力扩散。焊后随着放置时间的增加,焊缝金属中的含氢量下降,如果放置的时间足够长,则焊缝金属中的含氢量将会降低至接近于平衡值的水平。从图1中可以看出,焊后室温条件下放置40 d的焊缝金属进行刻槽锤断试验,断口表面的氢白点基本消失,断口呈韧性断裂。从表2中可以看出,焊缝金属中氢含量降低后,其-20℃冲击吸收功数据的离散度降低。从图3中可以看出,氢含量低的焊缝金属冲击断口形貌为韧性断裂。

## 4 结 论

(1) 采用自保护药芯焊丝焊接,药芯中氢含量较多而脱氢能力不足,熔池的存在时间相对较短,使得焊缝金属结晶时有相当多的氢来不及逸出。

(2) 在焊缝金属中含氢量较高的情况下,在氢和非金属夹杂物的共同影响下,低温冲击吸收功的平均值偏低,而且数据的离散度较大。

(3) 焊后放置时间为40 d,焊缝金属中的含氢量降低至接近于平衡值的水平,氢对焊缝金属冲击韧度的影响降低,刻槽锤断试样表面的氢白点减少或消失,低温冲击吸收功的平均值有所提高,并且数据的离散度降低,断口呈韧性断裂的比例增大。

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spot surface.

**Key words:** resistance spot welding; image of welding spot surface; image processing; Radical Basic Function neural network; quality monitoring

#### **Interface microstructure and mechanical property of CMT welding brazed joint between aluminum and galvanized steel sheet**

SHI Chang-liang, HE Peng, FENG Ji-cai, ZHANG Hong-tao (State Key Laboratory of Advanced Welding Production Technology, Harbin Institute of Technology, Harbin 150001, China). p61—64

**Abstract:** Welding-brazing experiment of aluminum and galvanized steel was conducted with cold metal transfer method. The interface microstructure and mechanical property of the joint were analyzed by SEM, EDAX and transverse tensile test. The results indicate that good lap joint between aluminum and galvanized steel sheet can be made in appropriate parameters. The interface turns to be thin from middle to the edge with the components changing from  $\text{FeAl}_3$  intermetallics to a compound of  $\alpha$  solid solution and  $\text{FeAl}_3$  intermetallics. Meanwhile, a rich-zinc zone composed of  $\alpha$  solid solution and aluminum at the edge of weld metal exists. In the tensile test, fracture appears in the heat affected zone of aluminum base metal, and its tensile strength is 72.09 MPa.

**Key words:** welding-brazing; cold metal transfer; intermetallics; interface; rich-zinc zone

#### **Numerical calculations of residual stress in Ti(C, N)/40Cr brazed joint**

WU Ming-fang, ZHOU Xiao-li, MA Cheng, YANG Pei (Provincial Key Lab of Advanced Welding Technology, Jiangsu University of Science and Technology, Zhenjiang 212003, Jiangsu, China). p65—68

**Abstract:** To obtain the effect of copper and molybdenum interlayer on the residual stress of Ti(C, N)/40Cr brazed joint, the finite element method was conducted. The simulation results showed that the high tensile stress concentration with a maximum stress magnitude of 268 MPa happens at the narrow zone near ceramic/steel seam in the ceramic side without interlayer, but when the metal with copper foil of low yield stress was used as interlayer, the residual stress can be significantly decreased, and the maximum residual tensile stress reduce to 98 MPa, and there are to change of maximum genetic zone in brazed joint with interlayer and without interlayer. When the low linear expansion coefficient metal molybdenum was used, the maximum stress occurred at the molybdenum interlayer zone, which gave a less residual stress reduction effect than copper foil. It also can be seen that the optimum interlayer thickness is about 0.8 mm for either interlayer kinds, and the thickness with thicker or thinner than 0.8 mm will be harmful to stress reduction effect.

**Key words:** Ti(C, N) based metal ceramic; 40Cr steel; brazing; residual stress; numerical calculation

#### **Effects of shielding gas on microstructure and number of gas pore in high strength aluminum alloys weld**

XU Liang-hong, TIAN Zhi-ling, ZHANG Xiao-mu, PENG Yun (State Key Laboratory

of Advanced Steel Processes and Products, Central Iron & Steel Research Institute, Beijing 100081, China). p69—73

**Abstract:** The effect of Ar and He dual mixed shielding gas and Ar, He and  $\text{CO}_2$  ternary mixed shielding gas on the number of the gas pore and microstructure in the weld was studied in arc welding of 2519 aluminum alloy. Results indicate that, compared with using Ar alone, the number and the size of gas pore is reduced by using Ar and He dual mixed shielding gas and the dual mixed shielding gas is also helpful for the transition of columnar crystal to equiaxed crystal. When the percentage of He reaches 70%, the number and the size of the gas pore are reduced significantly, and in weld centre it can get the smallest equiaxed crystal entirely. When filling 1%  $\text{CO}_2$  into the dual mixed gas which the ratio of Ar:He is 30:69, the number of the gas pore is further reduced, but there is no evidence to prove that it can affect the microstructure of the weld. The width and the softening extent of the HAZ can also be reduced by filling He into Ar shielding gas.

**Key words:** high strength aluminum alloy; mixed shielding gas; gas pore; microstructure

#### **Influence of hydrogen on weld metal toughness by self-shielded flux-cored wire welding**

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**Abstract:** The effect of hydrogen content on the low temperature toughness of weld metal was studied by Nick-Break test, low temperature impact test and scanning electron microscopy test, which filled by self-shielded flux-cored welding wire and held different periods in room temperature. The results show that all these conditions such as the high content of hydrogen in self-shielded flux-cored wire, uneasy outflow of hydrogen from the weld metal and the short-lived molten pool, make the content of hydrogen high in weld metal (immediately test after welding). The average value of impact absorbing energy at low temperature is low and the data are disperse under the action of hydrogen and non-metallic inclusion. When the work piece stored 40 days in room temperature, the content of hydrogen decreases and the fish eye decrease or disappear, and the average value of impact absorbing energy at low temperature increase and dispersion of the data decrease.

**Key words:** self-shielded flux-cored wire; pipeline; fish eye; impact absorbing energy

#### **Performance prediction in spot welding of body galvanized steel sheets based on artificial neural network and its optimization**

ZHAO Xin, ZHANG Yan-song, CHEN Guan-long, ZHANG Xiaoyun (School of Mechanical Engineering, Shanghai Jiaotong University, Shanghai 200240, China). p77—80, 84

**Abstract:** The performance prediction in spot welding of the galvanized steel sheets are very important in the automobile body manufacturing. So it was studied with galvanized steel sheet GMW2