

# Ti<sub>3</sub>Al 合金 TLP 扩散连接界面的组织演变

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**摘 要:** 以 Ti-37.5Zr-45Cu-40Ni(质量分数, %) 非晶箔带为中间层, 研究了 TLP 扩散连接 Ti-23Al-47Nb(质量分数, %) 合金的界面组织演变过程。结果表明, Ti 元素和 Nb 元素向中间层扩散而 Ni、Cu 和 Zr 元素向母材扩散驱动了界面组织演变; 在扩散初始阶段即 930 °C 保温 5 min 时, 界面已形成冶金结合; 随保温时间延长至 15 min, 界面析出条形 TiNi<sub>3</sub>(Cu, Zr) 化合物, 其随保温时间延长更加细小呈弥散分布; 直至保温时间延长至 120 ~ 200 min, 界面组织转变为均一、粗大的针状魏氏组织。保温时间是影响 TiNi<sub>3</sub>(Cu, Zr) 化合物析出形态和分布的主要因素, 控制保温时间可有效改变界面化合物状态, 该方法是优化此类界面组织以提高接头强度的有效途径。

**关键词:** Ti<sub>3</sub>Al 合金; TLP 扩散焊; 界面

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## 0 序 言

Ti-Al 合金具有较高比强度和比弹性模量、优良的抗蠕变和抗氧化性能, 适用于 650 ~ 750 °C 的环境, 是近年来重点开发和应用的航空航天用轻质高温结构材料<sup>[1-4]</sup>。目前在 Ti<sub>3</sub>Al 和 Ti<sub>2</sub>AlNb 合金的钎焊及瞬态液相扩散焊(transient liquid phase bonding, TLP)等技术方面已开展较多研究, 采用中间层合金或中间层包括镍基、钛基、银基及铜基合金, 采用钛基中间层合金或中间层时连接强度较高<sup>[5-9]</sup>。

有报道以 Ti-45Cu-45Ni(质量分数, %) 为中间层, 采用 990 °C 90 min 工艺 TLP 扩散连接 Ti-22Al-25Nb(质量分数, %) 的接头强度可达到母材强度的 95%<sup>[10]</sup>。但 Ti-45Cu-45Ni 中间层的熔点较高, 使连接温度较高、母材在焊接过程中易产生组织粗化, 不利于焊后材料的综合力学性能。添加 Zr 元素可有效降低中间层合金的熔点, 但导致界面形成化合物相—Ti<sub>2</sub>Ni, Ti(Cu, Al)<sub>2</sub> 成为接头脆性的主要因素。有报道指出<sup>[11]</sup>, 采用含 Zr 元素中间层和合理 TLP 扩散焊工艺, 可获得与采用无 Zr 元素中间层(即 Ti-Zr-Ni)等强度的焊接接头。因此适当添加 Zr 元素含量的中间层和合理的连接工艺应是控制接头脆性相和提高接头强度的有效途径, 且有利于兼顾焊后材

料的综合力学性能。

以 Ti<sub>3</sub>Al 合金——Ti-23Al-47Nb(质量分数, %) 为试验材料, 以 830 ~ 840 °C 熔点的 Ti-37.5Zr-45Cu-10Ni(质量分数, %) 非晶箔带为中间层, 观察 TLP 扩散连接界面微观组织, 分析中间层合金元素的扩散情况, 研究得出界面组织的演变规律, 为 TLP 扩散焊工艺的制定提供依据。

## 1 试验方法

试验中母材名义成分为 Ti-23Al-47Nb(质量分数, %) 室温组织由 α<sub>2</sub> 相、B<sub>2</sub> 相和 O 相组成, α<sub>2</sub> 相弥散分布于 B<sub>2</sub> 相基体上, 微量 O 相分布于 α<sub>2</sub> 相和 B<sub>2</sub> 相界面处。合金的退火工艺为 1 020 °C 3 h, 空冷, 室温抗拉强度为 966 MPa。以熔点在 830 ~ 840 °C 的非晶箔带 Ti-37.5Zr-45Cu-40Ni(质量分数, %) 为试验用中间层合金。在低于母材退火温度而高于中间层熔点的温度范围, 使用真空钎焊炉进行 TLP 扩散焊, 工艺为 800 °C 30 min + 930 °C (5, 15, 30, 60, 120, 200 min), 真空度不低于 10<sup>-3</sup> Pa。

界面组织观察用焊接试样规格为 φ10 mm × 5 mm, 接头强度测试用焊接试样规格为 φ10 mm × 35 mm, 中间层规格为 φ10 × (0.04 ~ 0.05) mm, 采用对接方式进行。用线切割方法将焊后试样沿轴向中心线切开, 使用水砂纸研磨线切割面至粗糙度达到 0.08 μm, 然后腐蚀该研磨面。采用扫描电子显

显微镜观察连接界面的微观组织形貌,采用电子探针分析界面元素的分布,参考试验结果评价界面组织均匀性,得出界面组织的演变规律,并通过透射电子显微镜对焊后界面的生成物进行鉴定,讨论生成相对界面强度的影响。

## 2 试验结果与分析

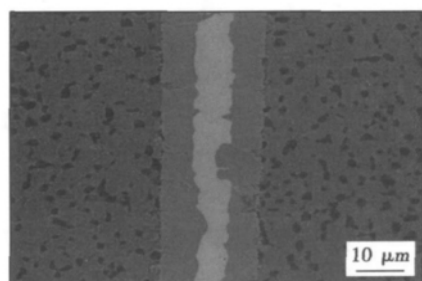
### 2.1 界面微观组织和元素扩散

图 1 所示为 930 °C 时 TLP 扩散连接界面的微观组织形貌。图 1a 为保温时间 5 min 时中间层合金与母材形成的冶金结合界面,中间层合金由 Ti、Zr、Cu 和 Ni 4 种元素组成,由于在背散射电子下原子量较大元素富集区的衬度较大,因而该温度下中间层凝固后元素偏析严重,界面中心部位富集 Zr、Cu 和 Ni 元素,但母材未发生组织明显变化;图 1b 为保温时间 15 min 时连接界面宽度约 40  $\mu\text{m}$ ,可见部分熔融

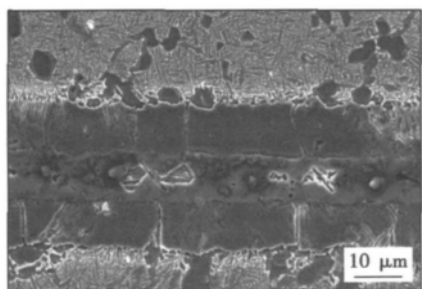
态的中间层合金组织,即残留液相层;图 1c 为保温时间延长至 30 min 时,液相层已经完全消失,界面宽度增至约 50  $\mu\text{m}$ ,即中间层的扩散程度显著增加。由图 1b、c 可见,在保温时间 15 min 和 30 min 下,中间层凝固后均由两种衬度的组织组成,即以富集 Zr、Cu 和 Ni 元素的为基体,富集 Ti 元素的深黑色组织弥散分布于其内;长时间保温下,灰白色组织向母材以树枝状形态扩展,其界面合金元素的扩散尚不充分,界面组织也不均匀。

图 2 所示当保温时间分别延长至 60、120、200 min 时,界面为钛基中间层合金经 TLP 扩散焊后形成的( $\alpha + \beta$  相)魏氏组织,而 Zr 元素的富集区演变为界面中心的狭长区域,宽度为 10  $\mu\text{m}$ ,此时界面组织均匀,TLP 扩散焊过程基本完成。

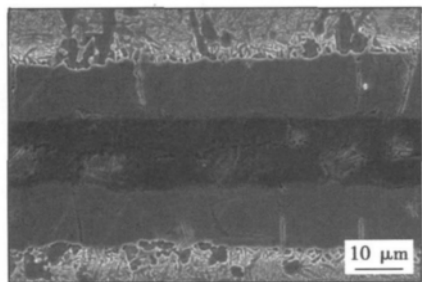
采用电子探针对 930 °C、60 min 下连接界面元



(a) 保温时间 5 min

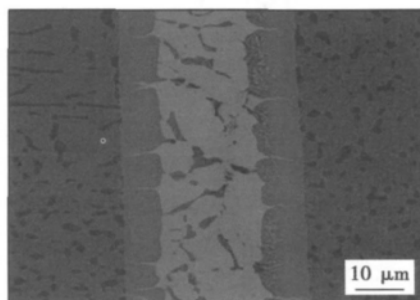


(b) 保温时间 15 min

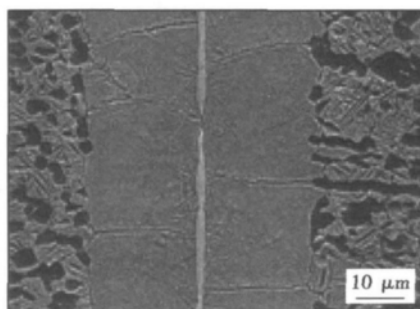


(c) 保温时间 30 min

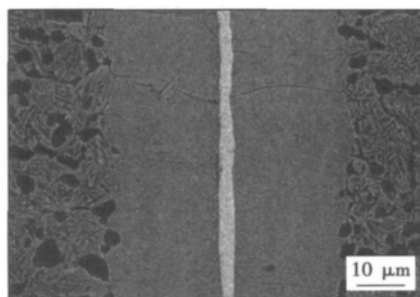
图 1 930 °C 下 TLP 扩散连接界面的微观组织形貌  
Fig. 1 TLP diffusing interface microstructure at 930 °C



(a) 保温时间 60 min



(b) 保温时间 120 min



(c) 保温时间 200 min

图 2 930 °C 下 TLP 扩散连接接头微观组织演变过程  
Fig. 2 Evolution processing of TLP diffusing interface microstructure at 930 °C

素含量进行分析,如图3所示。结果发现,Ti和Nb元素由基体向界面扩散,Zr,Cu和Ni元素由中间层向基体扩散,对比各元素由母材至界面中心的含量变化得出,Zr元素扩散对界面演变起到主要作用,如图4和表1所示。

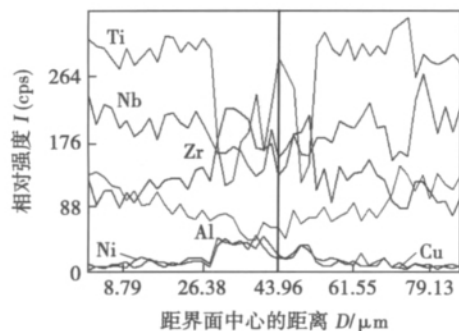


图3 界面元素分布(黑线为界面中心)

Fig. 3 Element distributing at welded interface

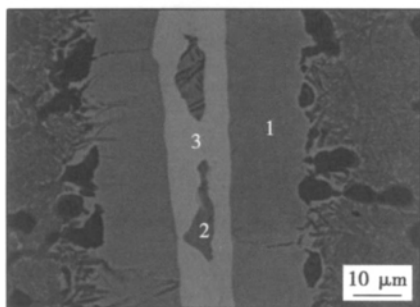


图4 中间层合金组织

Fig. 4 Solder microstructure

表1 界面化学成分(质量分数, %)(相应图4)

Table 1 Element content at welded interface

位置	Al	Ti	Ni	Cu	Zr	Nb
1	5.91	56.39	2.47	2.88	8.05	24.29
2	4.26	58.18	1.61	7.53	9.96	18.45
3	5.59	27.65	15.36	15.88	32.30	3.23

## 2.2 中间层焊后组织分析

在以上组织演变过程中存在两种典型组织,分别是930℃,60 min和930℃,200 min下界面组织。其中,930℃,60 min的连接界面内可见细小、弥散分布的析出物。析出物尤其是化合物对界面可能产生不利作用,这与化合物的种类和晶体结构有关。

采用X射线获得界面组织的电子衍射花样,如图5所示。分析得出,中间层经930℃,60 min焊后形成了六方晶体结构相和bcc晶体结构相,分别为 $\text{TiNi}_3(\text{Cu}, \text{Zr})$ 化合物和钛基固溶体。呈六方晶体结

构的 $\text{TiNi}_3$ 化合物中富集Zr,Cu和Ni元素,为灰白色相;而钛基固溶体为黑色相。据此可推测,随着保温时间由60~200 min延长,钛基固溶体与扩散区内元素的进一步充分扩散形成了图2b,c中的粗大针状组织的扩散区,即( $\alpha + \beta$ )魏氏组织。

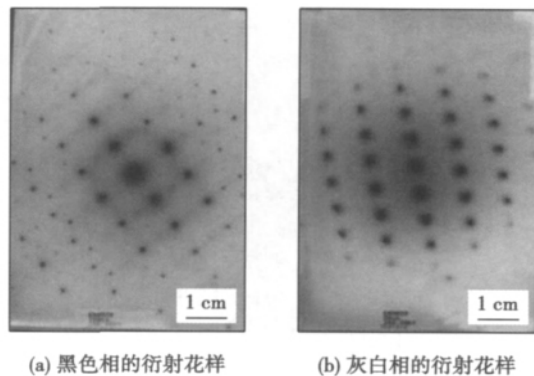


图5 界面上中间层的X射线衍射花样

Fig. 5 Diffraction pattern of solder at interface by X-ray

$\text{TiNi}_3(\text{Cu}, \text{Zr})$ 化合物会不利于接头的韧性,而具有bcc结构的钛基固溶体具有较好的塑性。这两种相的尺寸和分布情况将是该TLP工艺下接头强度和塑性的主要影响因素。当化合物尺寸较大、或分布不均匀时,加剧接头脆化,而当化合物相尺寸细小、且弥散分布时,可降低脆性化合物对接头性能的不利影响。

## 3 结 论

(1) 界面组织演变过程包括以下4个阶段:冶金结合界面形成、中间层残留液相消失、界面化合物析出和界面组织均匀化完成。

(2) Ti元素和Nb元素向中间层扩散而Ni,Cu和Zr元素向母材扩散驱动了界面组织演变。

(3) 保温时间是影响界面 $\text{TiNi}_3(\text{Cu}, \text{Zr})$ 析出物形态和分布的主要因素,通过控制保温时间可有效改变界面化合物状态。该方法可成为优化界面组织以提高接头强度的有效途径。

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SiO<sub>2</sub> , TiO<sub>2</sub> , CaF<sub>2</sub> , Cr<sub>2</sub>O<sub>3</sub> and BaCl<sub>2</sub>. The mechanism to increase weld penetration was analyzed by considering the change of arc shape in A-TIG welding process. The experimental results indicate that all the above activating fluxes improve weld penetration. The most remarkable effect is obtained when the flux is SiO<sub>2</sub> , but the effect of CaF<sub>2</sub> on penetration is not obvious. The weld appearance is poor when the base metal is coated with SiO<sub>2</sub> , while good weld appearance can be obtained when the flux of TiO<sub>2</sub> is used. The phenomenon of arc contraction is not remarkable when the arc moves into the flux zone. The significant improvement of weld penetration may be the result of increase in heat input caused by the change of resistance in conducting channel.

**Key words:** aluminum alloy; A-TIG; activating flux; weld morphologies

#### **Analysis of bending property of dissimilar steels welded joints**

WANG Rui<sup>1</sup> , WANG Fenghui<sup>2</sup> , TIAN Huaming<sup>3</sup> , ZHI Derui<sup>1</sup> , SUN Jie<sup>3</sup> , DU Jianfeng<sup>3</sup> , WANG Xibao<sup>2</sup> ( 1. School of Science , Tianjin University of Commerce , Tianjin 300134 , China; 2. School of Materials Science and Engineering , Tianjin University , Tianjin 300072 , China; 3. The Tianjin University Beiyang Chemical Equipment Co. , Ltd , Tianjin 300072 , China) . pp 58 – 62

**Abstract:** The dissimilar steel welded joints were made between Q235-B carbon steel and 316L stainless steel by submerge arc welding using Y and I patterns of welding groove. Based on the observation and analysis of the microstructure , elements distribution and micro hardness in the weld fusion zone near the Q235-B base metal , the hard and brittle transition layer would form in the fusion area near the carbon structural steel , when the dissimilar steels were welded. The decrease of width of brittle transition layer is the most important to improve the bending property of the dissimilar steels welded joint. Furthermore , the influences of different welding procedures on the bending property of the welded joint were investigated. The process of Y pattern groove and Ni-riched welding wire can minimize the width of brittle transition layer and raise the bending property of the welded joint. Besides , this welding procedure also avoids the welding fault of burning through when the butt joint of the dissimilar thin steel was welded by submerged arc welding on the double sides.

**Key words:** welded point; dissimilar steel; brittle transition layer; bending property

#### **Synchronous acquisition and analysis of metal transfer images and electrical parameters in CO<sub>2</sub> arc welding**

JIANG Yuanning , CHEN Maoai , WU Chuansong ( Institute for Materials Joining , Shandong University , Jinan 250061 , China) . pp 63 – 66

**Abstract:** By using high speed camera and multi-channel sensing and data acquisition system , a LabVIEW-based system was developed to acquire metal transfer images and electrical parameters in short circuiting CO<sub>2</sub> arc welding. The difference in startup delay time between data acquisition system and high speed camera was calibrated by experiment , and the offset by

software method to realize synchronous acquisition. The system was used to analyze the electrical parameters and metal transfer images. Metal transfer under different welding conditions was investigated and the correlation between electrical parameters , metal transfer image and the stability of short-circuiting transfer process was analyzed with the developed system.

**Key words:** CO<sub>2</sub> arc welding; virtual instrument; synchronous acquisition

#### **Growth mechanism of in situ Ti( C<sub>y</sub>N<sub>1-y</sub>) particles in laser deposited coating**

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**Abstract:** A new in-situ synthesis method was used to prepare the composite coating reinforced by Ti( C<sub>y</sub>N<sub>1-y</sub>) particles through CO<sub>2</sub> laser cladding technology. Scanning electron microscope ( SEM) and electron probe microscopy analyzer ( EPMA) were used to analyze the phases in the composite coating. The results show that Ti( C<sub>y</sub>N<sub>1-y</sub>) particles are formed by an in-situ metallurgical reaction of TiN particle and graphite powder during laser cladding process. The nucleation and growth mechanism of the formation of Ti( C , N) particles have close relationship with the original titanium nitride ( TiN) . When the size of the original titanium nitride particles is small ( < 5 μm) , a great deal of energy absorbed by the cladding material may cause the dissolution of the original titanium nitride ( TiN) particles to form the titanium carbonitride Ti( C<sub>y</sub>N<sub>1-y</sub>) particles , whose shapes are rhombus. If the size of original titanium nitride particles is big ( > 5 μm) , energy absorbed by the cladding material is limited , so it only causes the outer marginal dissolution of the original titanium nitride ( TiN) particles. Finally , the annular structure ceramic particles named titanium carbonitride Ti( C<sub>y</sub>N<sub>1-y</sub>) are synthesized by a solid-solution metallurgical reaction in the laser cladding process.

**Key words:** Ti( C<sub>y</sub>N<sub>1-y</sub>) ; in-situ formation; laser cladding; microstructure

#### **Microstructure evolution of TLP bonding interface for Ti<sub>3</sub>Al based alloy**

JING Yongjuan , LI Xiaohong , HOU Jinbao , YUE Xishan ( Beijing Aviation Manufacturing Engineering Research Institute , Beijing 100024 , China) . pp 71 – 74

**Abstract:** With Ti-37. 5Zr-15Cu-10Ni ( % ) amorphous foil as the brazing filler metal , the microstructure evolution of the TLP( Transient liquid phase) diffusion bonding interface for Ti<sub>3</sub>Al-based alloys was studied. The Ti and Nb elements diffuse into the brazing filler and the Ni , Cu , Zr elements diffuse into the matrix to drive the interface evolution. At 930 °C the metallurgical bonding is achieved after holding time of 5 min. The Ti-Ni<sub>3</sub>( Cu , Zr) compound in the shape of strip is precipitated after holding time of 15 min. This compound will get refined and dispersed with the holding time being longer. When the holding time lasts until to 120-200 min , the interface microstructure evolved to the coarse and homogeneous Widmanstatten structure. Since the compound character is affected by the holding time , it can be an effective method to control the microstructure and

strengthen the interface by controlling the holding time.

**Key words:**  $\text{Ti}_3\text{Al}$ -based alloy; transient liquid phase diffusion bonding; interface

**Measurement of creep stress exponent of Zn-Al filler metal at room temperature by using nanoindentation** JI Feng<sup>1</sup>, XUE Songbai<sup>1</sup>, LIU Shuang<sup>1</sup>, LOU Jiyan<sup>2</sup>, LOU Yinbin<sup>2</sup> ( 1. College of Materials Science and Technology, Nanjing University of Aeronautics and Astronautics, Nanjing 210016, China; 2. Zhejiang Xinrui Welding Material Co., Ltd, Shaoxing 312400, China ). pp 75 – 78

**Abstract:** The creep behavior of Zn-22Al and Zn-22Al-0.03Ti filler metals at room temperature were studied by nanoindentation in this paper, and constant loading rate method was used to calculate the creep stress exponent. The results indicate that, both the Zn-22Al and Zn-22Al-0.03Ti produced obvious creep deformation under holding load. Both the depth and creep displacement of Zn-22Al-0.03Ti were less than that of Zn-22Al, and the maximum difference were 15.68% and 26.87%, respectively. Under the constant time, the filler metals produced different creep displacement with different loadings. The creep stress exponents of two filler metals at room temperature were obtained by fitting method. Zn-22Al-0.03Ti had a higher creep stress exponent than Zn-22Al filler metal, which implied that Ti-bearing filler metals had better creep resistance than Zn-22Al alloy. The grain of Zn-22Al filler metal could be refined remarkably with the Ti addition, which might result in the increase of grain boundary and finally enhanced the creep resistance of alloy.

**Key words:** nanoindentation; Zn-Al filler metal; creep; creep stress exponent

**Structure and mechanical properties on DH40 ship building steel joints by multi-layer and multi-pass welding technology**

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**Abstract:** The weldability experiments of DH40 ship building steel were carried out by using the flux-cored wire  $\text{CO}_2$  gas shielded multi-pass welding technology. The microstructure and mechanical properties of the joint were studied systematically and the impact toughness was discussed, especially the reason why the impact toughness at HAZ of 5 mm from fusion line of weld root decreased greatly. The results showed that the tensile strength of joints is higher than that of the base metal of 575 MPa. All the samples used in the bending test are qualified and meet the plasticity requirement. The brittleness band is easily formed at HAZ, 5 mm from the fusion line at the weld root. The effect of microstructure heredity results in the coarse crystal grain, which is the secondary reason for the impact ductility decreasing, and the basic reason is the formation of a large amount of granular bainite.

**Key words:** DH40 steel; multi-pass welding technology; mechanical properties; microstructure

**Effect of process parameters on mechanical properties of friction stir welded Al-Li alloy lap joints** ZHANG Dan-

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**Abstract:** Through analyzing the microstructure and testing mechanical properties of friction stir welded Al-Li alloy lap joints, the effect of FSW welding parameters on the tensile properties of the lap joints was investigated. The results showed that the length of stir pin has significant influence on the tensile properties of lap joints. When the length of pin is changed from 2.8 mm to 2.5 mm, the ultimate strength and elongation of lap joints are obviously improved. Furthermore, the rotation speed / welding speed ( $\eta$ ) also affected the performance of joints. When there was a small increasing in  $\eta$ , the tensile properties of lap joints increased accordingly. For the Al-Li alloy lap structure, the optimum tool rotational speed is 800 r/min, welding speed is 200 mm/min and the length of pin is 2.5 mm, the ultimate strength of lap joint reaches 467 MPa, which is equivalent to 94% that of the base metal and the elongation is 3.18%. In addition, the analysis of tensile fracture appearance indicated that the tensile cracks initiate from the location of "Hooking" defect in the advancing side and grow along the HAZ until to the base metal.

**Key words:** friction stir welding; aluminum-lithium alloy (Al-Li); tensile properties; fracture

**Test and analysis of dynamic process for spot welding of multilayer low carbon steel sheets** LI Guizhong, DING

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**Abstract:** In the spot welding process, the spot-welded joints of multilayer sheets were always available. The variation of the sheet thickness is obvious in the spot welding process, which makes the impedance fluctuation drastic in secondary circuit of welding power transformer. Thus, the spot welding heat also fluctuates evidently. In this case, the nugget quality cannot be guaranteed if welding heat is not regulated effectively in real time. By means of dynamic test and analysis of welding thermal process, the applicability of different monitoring methods was discussed for spot welding of multilayer low carbon steel sheets. The scientific basis therefore can be provided for manufacturing enterprises to select the exact monitoring method and to achieve the effective quality control.

**Key words:** low carbon steel; multilayer sheets; spot welding; dynamic process; monitoring method selection

**Numerical simulation of metal plastic flow in friction stir welding affected by pin shape** JI Shude<sup>1</sup>, MENG Qing-

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