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基于 PCA-SVM 方法的点焊质量评估

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摘 要:通过对电阻点焊过程电极位移和动态电阻信号的实时采集和时域特征分析,利用电阻信号动态特征刻画熔核形成不同阶段,从同步电极位移信号中提取9个特征参量建立输入样本数据集,以焊点接头抗剪强度作为焊点质量的评价指标,将 PCA(主成分分析)方法与传统的 SVM(支持向量机)回归分析相结合,利用 PCA 方法对支持向量机的输入样本数据集进行主成分分析,消除了输入特征参量间的自相关性。实现数据降维后作为支持向量机的输入,建立焊点质量映射模型。交叉有效性预测结果表明,基于 PCA-SVM 的算法增强了 SVM 的泛化能力,比传统的 SVM 算法具有更高的预测精度。关键词:电阻点焊;主成分分析;支持向量机;回归分析



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0 序 言

点焊过程是一个高度非线性、多变量耦合作用 的过程, 同时伴随着大量随机不确定因素, 焊点质量 不稳定,难以控制. 随着现代信号分析、数据处理技 术的迅速发展,利用点焊过程焊接电流、电极电压、 动态电阻、电极位移等动态信号特征分析进行焊点 质量评估受到广泛关注[1-3]. 但是应用传统机器学 习方法(如多元回归分析、神经网络等)实现回归分 析普遍采用经验风险最小化原则,在样本数目有限 时,需要同时最小化经验风险和置信范围,学习过程 无法避免过学习、维数灾难、局部最小等问题, 限制 了上述各种方法的应用. 支持向量机是建立在结构 风险最小化基础上的统计学习理论,有望解决传统 方法在机器学习中遇到的各种问题, 因此提出一种 基于点焊过程电极位移信号特征分析, 结合主成分 分析和支持向量机统计分析方法实现点焊过程多动 态信息融合及焊点质量评估的方法.

1 PCA-SVM 方法

多变量研究中,往往由于变量个数太多,并且彼此之间存在一定的相关性,使得所观测的数据在一定程度上反映的信息有所重叠.利用主成分分析¹⁹

可以通过降维,找到几个彼此互不相关的综合因子 来代表原来众多的变量,使这些综合因子尽可能地 反映原来变量的信息.

对于 n 维向量样本集 z_i ($i = 1, 2 \cdots n$), 定义样本的协方差矩阵为

$$S = \frac{1}{m} \sum_{i=1}^{n} - (z_i - \mu)(z_i - \mu)^{\mathrm{T}}$$
 (1)

式中: $\mu = \frac{1}{m} \sum_{i=1}^{n} z_i$. 对 S 进行正交分解, 前 k 个主元 $(k \le n)$ 所概括的原样本集的信息大小可由前 k 个主元的方差贡献率来表示, 即

$$\theta = \sum_{i=1}^{k} \lambda_i / \sum_{i=1}^{n} \lambda_i \tag{2}$$

式中: λ_i 是 S 矩阵按照降序排列特征值. 重构测量矩阵 Z = Z + Z, 其中 $Z = V_k P$, $V_k = [\nu_1, \nu_2 \cdots \nu_k]$ 为负荷矩阵, $\nu_i (i = 1, 2 \cdots k)$ 为特征值 λ_i 对应特征向量组成的特征矩阵; P 为主元矩阵; Z 为 Z 的残差. 这样前 k 个特征向量构成的 PCA 子空间就能提供 Z 样集的所有特征信息, 实现了 $Z^n \rightarrow Z^k$ 的降维.

回归分析可以归结为寻求最优回归超平面问题 等同于如下凸约束条件下的二次凸规划问题⁷¹,即

$$\min \left\{ \frac{1}{2} \parallel W^2 \parallel + C \sum_{i} (\zeta_i + \zeta_i^*) \right\}$$
 (3)

式中: W是线性函数系数, $W \in R^n$; 常数 C 为控制对超出误差 ε (控制回归逼近误差管道的大小) 样本的惩罚程度, 一般由试验确定; ζ_i , ζ_i^* 为松弛因子, 分别对应于最优回归超平面上方和下方的样本点.

式(3) 的约束条件为

$$y_{i} - (Wx_{i}) - b \leqslant \varepsilon + \zeta_{i}$$

$$(Wx_{i}) + b - y_{i} \leqslant \varepsilon + \zeta_{i}^{*} (i = 1, 2 \cdots n)$$

$$\zeta_{i}, \zeta_{i}^{*} \geqslant 0$$

$$(4)$$

式中: x_i , y_i 为 n 个观测样本; $b \in R$ 表示阈值.式(3)中引入拉各朗日乘子,可以得到其对偶问题,即在式(5)条件下,对拉格朗日因子 α_i , α_i^* 最大化目标函数见式(6),这样最优超平面的表达式为式(7),即

$$\sum_{i=1}^{n} (\alpha_{i} - \alpha_{i}^{*}) = 0$$

$$0 \leqslant \alpha_{i}, \alpha_{i}^{*} \leqslant C, i = 1, 2 \cdots n$$
(5)

$$W(\alpha_{i}, \alpha_{i}^{*}) = -\varepsilon \sum_{i=1}^{n} (\alpha_{i} + \alpha_{i}^{*}) + \frac{1}{2} \sum_{i=1}^{n} y_{i} (\alpha_{i}^{*} - \alpha_{i}) - \frac{1}{2} \sum_{i,j=1}^{n} (\alpha_{i}^{*} - \alpha_{i}) (\alpha_{j}^{*} - \alpha_{j}) (xx_{i})$$
(6)
$$f[\phi(x)] = \sum_{\text{with}} (\alpha_{i}^{*} - \alpha_{i}) (xx_{i}) + b$$
(7)

支持向量机统计学习方法通过在式(7) 中引入核函数 $K(x,x_i)$ 就可以实现非线性函数拟合.式(8) 为 SVM 非线性回归函数,即

$$f[\phi(x)] = \sum_{\text{tigh}} (\alpha_i^* - \alpha_i) K(xx_i) + b \quad (8)$$

SVM的核函数包括线性核函数、Sigmoid 核函数、高斯径向基核函数等,文中选用应用最广泛的高斯径向基核函数,如式(9)所示.

$$K(x, x_i) = \exp\left(-\frac{\|x - x_i\|^2}{r^2}\right)$$
 (9)

式中,r是核半径,代表着基函数的宽度.

2 电极位移信号的特征提取

试验信号采集系统由恒流控制方式的交流电阻点焊机、传感器、信号调理电路、A/D 转换器组成.针对0.7 mm 板厚的低碳钢板进行搭接点焊,电极压力2.0 kN,电极头工作面直径6 mm,焊接电流为3.2~4.4 kA之间,共60组试验样本,焊点质量利用接头抗剪强度评价,单位为 MPa. 图 1 是焊接电流4.4 kA,焊接时间20 周波采集到的一组动态电阻、电极位移同步信号波形,其中动态电阻信号通过焊接过程每半周波电流峰值时刻的电压值除以电流值获得,这样可以消除交流回路互感现象的影响,得到纯净的动态电阻值[8].

图 1b 是点焊过程电极位移信号曲线, 主要由加热膨胀、缓慢下降和冷却收缩三个阶段组成, 焊接开始的早期阶段电极没有明显位移, 从 2 周波后开始快速上升, 图 1b 中 d 点对应同步电阻信号的峰值时刻(与图 1a 中 b 点时刻对应), 大量研究认为动态电

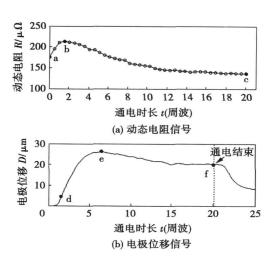


图 1 动态电阻和电极位移同步信号波形

Fig. 1 Original signal of dynamic resistance and electrode displacement

阻的峰值时刻标志焊点熔核的形成. 图 1b 中 e 点为位移峰值时刻. 峰值过后由于焊接区金属受热进一步软化,电极压痕逐渐加深,位移曲线开始缓慢下降直至通电结束(f 点时刻),通电结束后熔核液相金属结晶,位移曲线陡降.

针对位移信号变化的不同阶段,从信号中提取 出9个特征参量作为表征和评估焊点质量的相关因 \mathbf{F} , 其中 λ_1 表示位移峰值时间率(峰值时间 / 焊接 通电时间); D1表示峰值位移量, 这两个特征参量是 焊点金属熔化量的度量; D_2 表示位移信号峰值时刻 与断电时刻位移的变化量,以反映电极压痕深度的 变化: D3 表示半周波位移变化量最大值; D4 表示焊 接过程平均电极位移; ΔD 表示半周波位移标准差, 用以反映位移信号的变化趋势: v1 反映熔核形成的 平均速度,表示焊接通电开始到动态电阻达到峰值 时刻(图 1b 中 d 点)终止电极位移的平均上升速度; v₂ 反映熔核长大平均速度,表示电阻峰值时刻开始 到位移峰值时刻终止(图1b中d和e点之间)电极位 移的平均上升速度,当焊接电流较小时,焊接区加热 速度较慢,这两个速度相对较慢; 1/3 表示位移峰值 时刻开始到通电停止时刻终止(图 1b 中 e 和 f 点之 间) 位移的平均下降速度, 可以反映电极压痕由浅 到深的变化速度.

图 2 分别绘出了60 组试验样本所提取特征参量与焊点接头强度分布的散点图.

3 PCA-SVM 焊点接头强度预测

由干电极位移信号中所提取的各个特征参量数

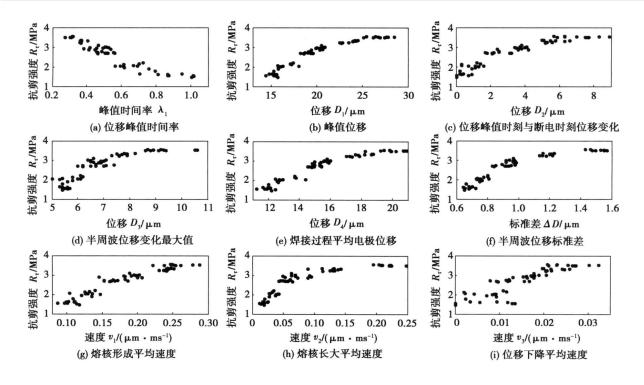


图 2 电极位移信号特征参量散点图

Fig. 2 Scatter diagrams for characteristic value of electrode displacement

量级和量纲存在较大差异,因此利用 PCA-SVM 统计分析方法进行焊点接头强度预测时,首先采用最大最小值方法对数据进行归一化处理,使得所有分量表示相对大小. 归一化后的数据空间构成矩阵. 对归一化后的数据矩阵进行主成分分析,分析结果如表 1 所示. 分析表明采用 PCA 算法,它的前 4 个主成分所对应的特征值依次为 0. 347 8 0. 013 1, 0. 009 8, 0. 004, 累计贡献率分别为 91. 895 2%, 95. 369 6%, 97. 967 9%, 99. 033%, 远远大于通常要求的 85%, 第 5 到第 9 个主成分贡献率可以忽略不计,数据降维效果理想.

表 1 主成分分析结果
Table 1 Results of PCA method

特征值序号	特征值λ;	贡献率 θ(%)	累计贡献率 α(%)
1	0. 347 8	91. 895 2	91. 895 2
2	0.0131	3. 474 4	95. 369 6
3	0.0098	2. 600 1	97. 969 7
4	0.004	1.063 3	99. 033
5	0.0019	0.4908	99. 523 8
6	0.001	0. 252 6	99. 776 4
7	0.0007	0. 185 2	99. 961 6
8	0.0001	0. 033 4	99. 995
9	0.000 02	0.005	100

文献[4] 提出了一种非常适合于小数据空间建立和测试数学模型有效性的方法: 依次取出每个数

据样本,用剩余的数据样本构建数学模型,之后用所取出的数据样本检验数学模型,最后将取出的数据样本放回,对整个数据空间每个样本都重复上述操作过程,在有效增加参与建模数据样本数量的同时也增加了测试样本的数目.试验所建立的监测模型有效性检验借鉴这种方法.

利用主成分 1 至 4 重新构建表征焊接过程数据集(60×4 数据矩阵)并作为高斯径向基支持向量机的输入,以焊点接头抗剪强度为输出,采用上述交叉有效性检验方法检验 PCA-SVM 回归分析预测效果.为了进一步了解 PCA-SVM 方法的预测效果,试验单独采用 SVM 统计分析方法对未经主成分分析的原始 60×9 数据集进行高斯径向基支持向量机回归分析,并对两种方法交叉有效性测试结果进行比较.

对于给定的样本, 支持向量机的推广能力主要受到核函数(如径向基核函数中的核半径 r, 它对模型的预测精度有重要影响)、回归管道宽度 ε 和惩罚参数 C(用于控制模型复杂度和逼近误差的折中)的影响^[8]. C 越小, ε 越大, 支持向量越少, 模型简单, 推广能力好, 但数据拟合精度可能较低, C 越大, ε 越小, 模型复杂, 数据拟合精度提高, 但可能导致推广能力降低. 理想的模型应该是在适当的拟合精度下具有较强的推广能力. 因而相关参数确定本身也是一个复杂的优化问题.

目前对于支持向量机参数优化的方法多用交叉验证法、网格搜索法、遗传算法等处理. 试验采用网格搜索法得到一组较优的参数设置,其中核半径 *r* 为 0.89,惩罚因子和管道宽度分别取 1 000 和 0.001时预测结果较好.

图 3 为两种方法的预测结果, 表 2 给出了两种方法预测相对误差的比较, 结果表明 PCA-SVM 体现出更强的泛化能力.

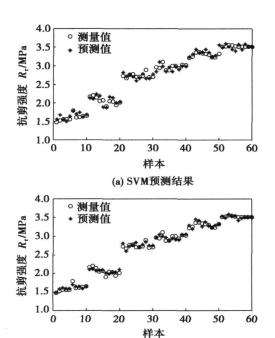


图 3 PCA SVM 和 SVM 接头强度预测结果

(b) PCA-SVM预测结果

Fig. 3 Tensile shear strength prediction results of welded spot joint with SVM and PCA-SVM method

表 2 PCA SVM 和 SVM 接头强度预测误差

Table 2 Prediction error of shear strength of welded spot joint

预测方法	最小误差	最大误差	平均误差	均方误差
	$e_{\min}(\%)$	$e_{\mathrm{max}}(\%)$	$e_1(\%)$	$e_2(\%)$
SVM	0.02	10. 43	3.99	4. 80
PCA-SVM	0.02	5.5	1.95	2. 42

4 结 论

- (1) 利用 SVM 和 PCA-SVM 统计分析方法均可以较为有效地实现焊点接头抗剪强度的预测,表明提出的结合动态电阻、电极位移同步信号特征分析刻画焊点熔核形成不同阶段的方法是有效的.
- (2) 将 PCA 方法与传统的 SVM 回归分析相结合,利用 PCA 方法对支持向量机的输入样本数据集进行主成分分析,可以有效削减样本空间的维数并消除了输入变量间的自相关性,交叉有效性预测结果表明,结合 PCA 和 SVM 的算法增强了 SVM 的泛化能力,比传统的 SVM 算法具有更高的预测精度.

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(State Key Laboratory of Advanced Welding Production Technology, Harbin Institute of Technology, Harbin 150001, China). p93—96

Tensile strength, bending strength, impact tough-Abstract. ness and non-destructive inspection tests of TIG welded 20G/316L clad pipe joint were carried out. The microstructure and the diffusion of the major alloying elements were analysed using optical microscopy, SEM and chemical analysis. The results showed that the weld can be divided into four layers including carbon steel layer, diffusion layer, transition layer and stainless steel layer. The microstructure in diffusion layer was characterized by the marten site and retained austenite. The transition layer only contained austenite and the stainless steel layer included afterbirth-like crystal. The defectfree joint was produced and performed well under the experimental parameters. The concentration of nickel and chromium element in weld not did not decrease compared with the corresponding welding materials, which proved that the employment of transition welding wire could maintain the concentration of the major alloying elements in welding root.

Key words: 20G/316L clad pipe; TIG; microstructure; mechanical properties

Quality evaluation of the resistance spot welding based on PCA-SVM ZHANG Hongjie¹, HOU Yanyan²(1. School of Machinery and Electron, Tianjin Polytechnic University, Tianjin 300160, China; 2. Department of Architecture Engineering, Hebei College of Administration, Shijiazhuarg 050031, China). p97—100

Abstract: The electrode displacement and dynamic resistance signals of resistance spot welding process are collected synchronously. Through the time-domain analysis of electrode displacement signal in the welding process, nine characteristic parameters relating to weld quality are picked up to set up a set of data which characterizes the input samples, on the basis of the different phase of nugget forming marked by simultaneous dynamic resistance signal. The principal component analysis (PCA) to remove the self-correlation of input characteristics and realize dimensionality reduction is integrated with the conventional method of support vector machine (SVM), while the shear strength of welded spot was taken as the evaluation index of welded spot quality. The comparison of predicted results under PCA-SVM and conventional SVM by means of cross-validation test shows that PCA-SVM algorithm improves the generalization ability and the predicted accuracy of SVM method.

Key words: resistance spot welding; principal component analysis; support vector machine; regression analysis

Numerical simulation of the temperature field during resistance spot welding with rectangular electrode ZHANG Xiaoqi^{1, 2}, XU Guocheng¹, WANG Chunsheng^{1, 3}, WEN Jing¹ (1. School of Material Science and Engineering, Jilin University, Changchun 130025, China; 2. Jilin Teachers Institute of Rnqineeriy and Fechnology, Changchen 130052, China; 3. Changchun Railway Vehicles Corporation, Changchun 130062, China). p101—104

Abstract: The temperature field during resistance spot weld-

ing with rectangular electrode was simulated using ANSYS. The physical model was properly simplified on the basis of simulation accuracy and technological conditions. One quarter three-dimensional finite element model during resistance spot welding was built in which the contact resistance was substituted by the electric resistivity. The results show that at the beginning of welding, the edge of electrodes has the highest temperature because of high stress induced by the electrode force. As welding time is longer, the contact resistance decreases and the highest temperature position moves to inside, the nugget appears to be similar with the conventional spot welding.

Key words: rectangular electrode; numerical simulation; temperature field

Laser-based visual recognition of multi-pass seam in robot arc welding ZHANG Huajum^{1, 2}, ZHANG Guangjum¹, CAI Chumbo², GAO Hongming¹, WU Lin¹ (1. State Key Laboratory of Advanced Welding Production Technology, Harbin Institute of Technology, Harbin 150001, China; 2. College of Material Science and Engineering, Harbin University of Science and Technology, Harbin 150040, China). p105—108

Abstract It is very necessary for the improvement of weld quality and the realization of robot automatic production to detect multi-pass weld profile parameters automatically. Automatic detective system of multi-pass weld profile parameters by band laser visual sensor was developed. The procedure of image process is as follows; smoothing, center recognition by longitudinal grey gradient, twice slope smooth process, and multiple peaks search by laser seam image analysis. It is very important for seam tracking, arc length control and torch attitude adjustment to obtain four character points of weld seam profile. And the recognition results agree with the experimental results.

Key words: multipass welding; laser visual sensor; image process; twice slope smooth process; robot arc welding

Research on gravity compensation algorithm for tool-assembling with force control in remote welding WEI Xiuquan, WU Lin, GAO Hongming. II Haichao (State Key Laboratory of Advanced Welding Production Technology, Harbin Institute of Technology, Harbin 150001, China). p109—112

Abstract Based on the control strategy of global teleoperative and local autonomous a tool-assembling experimental system with force control for remote welding is established. The tool gravity calculation and linear least-squares algorithm are adopted to calibrate the tool load parameter, and a tool gravity compensation algorithm based on the tool load parameter vector is proposed to eliminate the gravity disturbance during the tool-assembling process with force control. For a customized assembing tool, experiments on load parameter calibration and gravity compensation in non-contact condition are carried out. The experimental results show that the tool gravity compensation algorithm can obtain a high precision, meeting the requirements of local autonomous force control in tool-assembling task, while the maximum error of gravity compensation and gravity moment compensation are 1 N and 0. 1 Nom, respectively.

Key words: gravity compensation; force control; tool assembling; remote welding