# 全数字控制 I/I 模式三闭环脉冲 MIG 焊

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摘 要: 提出了一种基于 DSP 控制的全数字脉冲 M IG/ MAG 控制方法. 即自适应电压补偿控制技术的 I/ I法,该方法可以保证熔滴为一脉一滴过渡. 根据送丝速度优先,建立不同材料和丝径的焊接数据库,每个脉冲周期都检测弧长的变化并及时调整熔化能量,同时采用干伸长实时补偿技术以维持弧长恒定.分析了该方法调节原理并建立三闭环系统控制框图. 样机试验结果表明,所提出的方法是可行的,具有通用性,在干伸长变化时能够实现等弧长控制,焊接过程稳定,焊缝成形美观.

关键词: 脉冲 MIG 焊; 全数字控制; 弧长

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## 0 序 言

熔化极脉冲焊时,脉冲峰值和基值交替产生,主 动控制熔滴的过渡,能量大小本身可控且能量给予 的时刻可控.与短路过渡方式相比,该方法有以下优 点.(1)可以在很宽的全电流范围内实现射滴过 渡,焊接时无飞溅或飞溅很小. (2) 可以焊接多种 材料,精确控制热输入量,不仅能焊钢、不锈钢等黑 色金属,还能焊接铝、铜、镍等有色金属. (3)更容易 实现全位置焊接,采用脉冲电流、可用较小的平均电 流进行焊接,因而熔池体积小,熔滴过渡和熔池金属 的加热是间歇性的,不易发生淌流,可顺利完成横 焊、立焊. 正因为以上优点, 在很多工业应用场合如 铝合金或不锈钢的高速列车车体的焊接、航天、轮船 制造中,脉冲焊被广泛使用. 在峰值电流阶段产生 很大的电磁力克服表面张力的束缚,熔滴过渡,在基 值阶段维持电弧的稳定燃烧,形成熔滴. 在峰值阶 段要有足够的电磁力克服其表面张力,由脉冲的峰 值电流的大小和其维持的时间决定[1],在脉冲峰值 阶段, 阴极斑点数量远大干基值电流期间, 所以脉冲 峰阶段的电压能够代表弧长信息.

对于脉冲 MIG/MAG 的控制,从输出电压或电流的特性而言主要有以下方法. (1) 压频转换型输出平均电压恒定型 $^{(2)}$ . (2) U/I 模式,即峰值电压

式,即峰值电流和基值电流保持恒流特性. 方法(1) 认为输出电压的平均值表征了弧长信息,但是滤波 以后, 弧长信息采集滞后, 压频转换采用模拟电路产 生, 电阻和电容值的选取很难兼顾小电流和大电流. 方法(2)抗弧长扰动能力强,但是当干伸长变化,无 法保证过渡能量满足要求. 当干伸长增加, 峰值电 流减小,有可能导致峰值能量满足不了射流过渡要 求. 当干伸长减小, 峰值电流增加, 峰值能量太高, 导致一脉多滴. 该方法的另一个缺点,很难实现复 杂的波形变化,如对于不同的材料脉冲上升的斜率 和下降斜率是不同的,由于滤波电感的滞后效应,脉 冲电压和电流并不是完全同相位的, 因此脉冲的波 形控制实现复杂. 方法(3)可以在任何情况下满足 射滴过渡的要求,使得熔滴一脉一滴可靠过渡,且可 以随意控制脉冲上升和下降斜率. 如果电源输出的 峰值电压不变, 当干伸长增加, 因为峰值电流不变, 则电弧压降变小,则弧长降低,而当干伸长减少,电 弧压降变大,则弧长增加. 可见采用传统的 I/I 模 式, 当干伸长变换时, 无法维持弧长的恒定.

保持不 变, 基值 电流保持恒 流特性[3]. (3) I/I 模

### 1 自适应电压控制 I/I 模式的原理

结合 I/I 和 U/I 模式的特点,提出自适应电压控制的 I/I 脉冲 M IG 焊方法,该方法结合了两种方法的优点,在确保一脉一滴过渡的情况下,能够自动适应干伸长的变化,保持弧长的相对恒定。但事实上电弧电压不可直接测量,输出电压可描述为

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 $U = R_{\omega}I + \rho_{\rm r}l_{\rm s}I + U_0 + R_{\rm a}I + E_{\rm a}l_{\rm a}$  (1)

式中: I 为输出电流;  $R_{o}$  为输出电缆和接触电阻;  $\ell_{r}$  为焊丝单位长度电阻;  $l_{s}$  为干伸长;  $U_{0}$  为电势常数;  $R_{a}$  为电弧电阻;  $E_{a}$  为描述弧长和电弧压降的常数. 输出电压包含了干伸长压降和电弧压降. 焊接本质上是一种多状态变量的非线性、时变和强耦合系统<sup>41</sup>,计算干伸长实时变化的理论模型还需要实践的检验<sup>51</sup>. 如何计算干伸长的变化是一个难题, 因为协同控制为送丝速度优先, 根据送丝速度设定焊接数据库, 而电弧稳定的前提条件是送丝速度和熔化率成正比, 而熔化率由干伸长电阻热和焊接电流决定, 即

$$M_{\rm R} = C_1 I + C_2 \rho_{\rm r} I^2 l_{\rm s} \tag{2}$$

式中:  $C_1$  和  $C_2$  为常数; I 是干伸长为  $I_s$  时稳定输出的焊接电流.

当干伸长由 /s 变化到 /s 的时候, 达到新的稳态, 此时熔化率描述为

$$M_{\rm RI} = C_1 I_1 + C_2 \rho_{\rm r} I_1^2 I_{\rm s1} \tag{3}$$

式中: $M_{\rm RI}$  为新的熔化率; $I_{\rm I}$  是干伸长为  $I_{\rm SI}$  时稳定 输出的焊接电流,因为设定的送丝速度不变,所以,  $M_{\rm RI} = M_{\rm R2}$ ,由式(2)和式(3)可知,当干伸长减小, 则输出电流减小,当干伸长增加时,输出电流增加. 所以焊接输出电流的变化反映了干伸长变化的趋 势, 因为峰值电流保持不变, 所以干伸长的压降和干 伸长长短成正比. 为了补偿干伸长的压降,对于峰 值电压的给定进行动态调整,该方法具有传统 I/I 模式脉冲 MIG/MAG 焊的特点, 即在峰值阶段保持 恒流,在基值阶段也维持恒流,具体调节过程如图 1 所示,在脉冲峰值阶段通过采样电压得到当前脉冲 周期的弧长变化信息。然后调整接下来的基值时间 和基值电流的大小,改变焊丝的熔化速度,让弧长恢 复到正常的值. 同时计算新的脉冲周期 $(t_1 \sim t_3)$ 的 电流平均值,根据设定的标准值进行比较,调节输出 的值来动态地改变峰值设定,将干伸长上的电压补 偿,从而保证电弧上的压降不变,弧长就可以保持不 变,采用该方法,不仅对干弧长的变化在一个脉冲周

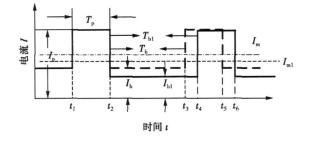


图 1 自适应电压补偿 // I 调节原理 Fig. 1 Regulation principle of AVC // I control

期进行响应,对于基值电流的大小和维持时间进行调整,而且下一个脉冲周期实现了干伸长压降的自动补偿.

整个控制系统的实现如图 2 所示,采用送丝速 度优先,根据材料和丝径,配制气体比例来选取能量 参数,如峰值时间、峰值电流、基值时间、基值电流. 框图由于伸长电压补偿器、弧长调节器和瞬时值电 流反馈控制环构成,是一个三闭环系统. 弧长调节 器输出不仅改变着基值电流的大小,也改变着基值 电流的时间,不断地切换峰值和基值之间的时序,完 成电流给定的切换. 最外环是具有干伸长压降补偿 功能自适应电压控制,其中 las 为设定弧长,通过对 于输出电流的离散积分运算得到实际的反馈弧长 laf, 经过比较运算, 进行自适应电压控制得到峰值电 压的给定  $U_{\text{peak}}$  与反馈峰值电压  $U_{\text{peak}}$  比较, 经过补 偿运算得到新的基值电流给定 Ubref 和峰值电流给 定,最内环为电流环,根据峰值时间和基值时间的时 序来切换电流环给定.  $K_2$  和  $K_1$  分别为电流环和电 压环的反馈系数,而  $\tau$  是弧长检测的时间常数,L 是 回路电感, S 是微分算子, A 是主电路放大倍数. 其 它的物理量定义同式(1).

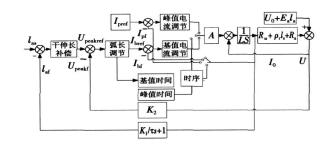


图 2 自适应电压补偿 // / 控制框图 Fig. 2 Block diagram of AVC // / control

### 2 试验结果

所有的控制算法均采用 TI 的 TMS320F2407型DSP完成,包括电压、电流的采样、三闭环数字补偿算法、数字化软开关 PWM 和数据通信.采用所提出的 AVC I/I 控制策略在设计的全数字化多功能焊接电源平台 Synergic400上进行了焊接试验.试验结果如图 3~图 5 所示.图 3 为下台/升台试验波形,台阶高度为 1.5 cm,送丝速度为 7 m/min,焊丝为铝镁 ф1.2 mm焊丝,保护气体为 100% 氩气.图 3a 为下台试验波形,由波形可知,下台以后,脉冲频率下降,脉冲峰值电压略有升高,补偿了干伸长上的压降.图 3b 为升台试验波形,升台以后,脉冲的频率增加,

而此时干伸长上压降变小,脉冲峰值电压略有下降, 由图 3a 和图 3b 可知, 在下台或升台前后, 脉冲频率 发生明显改变,波形稳定,没有出现异常短路和断弧 情况,焊接峰值电压能够自动调整以适应干伸长的 变化. 图 4 是采用该方法焊接铝镁合金电压电流波 形,其中图 4a 为整体电压和电流波形,图 4b 为展开

800 40 NA 400 -40 -80-400 100 200 300 400 500 600 700 800 900 时间 t/ms

(a) 下台试验

的电压和电流波形,试验条件为送丝速度3.5 m/min, 焊丝直径 1.2 mm, 保护气体 100% 氩气, 板厚 2.5 mm, 焊接的输出平均电流和电压分别为 59 A 和 16.8 V. 图 5 为该工艺参数下的实际焊接焊缝形貌, 从试验可 以看出, 焊缝纹理清晰, 致密, 边沿齐整, 熔合良好, 飞 溅小.

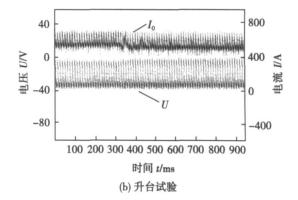
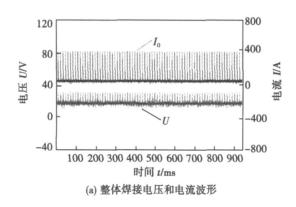


图 3 台阶试验电压和电流波形

Fig.3 Voltage and current waveforms of step experiment



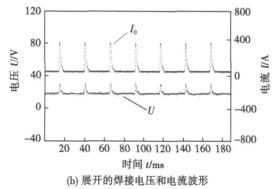


图 4 铝镁合金电弧电压和焊接电流波形

Fig. 4 Voltage and current waveforms of aluminum alloy



图 5 铝镁合金焊接焊缝形貌

Fig. 5 Appearance of aluminum alloys weldment

#### 结 论 3

(1) 提出的全数字化自适应电压控制的 I/I 控 制策略是可行的,在一个脉冲周期内,可以对弧长进 行快速调节,在干伸长变化时也能够保持弧长的相 对恒定.

- (2) 在干伸长突然变化时,脉冲频率自动调整, 同时电弧电压也自适应调整以补偿干伸长变化所引 起的压降变化.
- (3) 所提出的控制策略具有通用性, 焊接材料 适应性强,焊缝成形美观,飞溅小,熔合良好.

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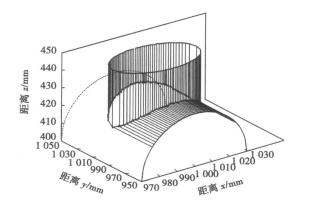


图 8 马鞍形焊缝结构的重建 Fig. 8 Reconstruction of saddle-shaped seam

### 4 结 论

- (1) 对于空间焊缝的双目立体视觉测量,采用极线约束简化了匹配点的寻找范围.
- (2) 采用激光标识, 一方面通过计算激光线与极线的交点确定匹配点, 准确性更高, 避免了可能产生的误配; 另一方面通过激光线上的奇变点检测可以准确计算焊缝的位置.
- (3) 对焊缝图像中激光线的提取、骨络化及去毛刺处理方法是有效的,保证了激光线的光滑.
- (4) 对直交圆管的空间马鞍形焊缝进行了检测和三维数据重建试验. 结果表明, 基于极线约束和激光标识的空间焊缝检测原理是可行的, 测量精度满足机器人自动焊接过程中的焊缝检测要求.
- (5) 文中采用的方法可以实现空间焊缝、周边结构及焊件结构形态的同时检测.

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### MAIN TOPICS, ABSTRACTS & KEY WORDS

Study on microstructure of the coatings sprayed in low pressure condition and its post treatment technology. LI Deyuan SONG Dan ZHANG Zhongli ZHAO Lingvan (School of Materials Science and Engineering Shenyang University of Technology, Shenyang 110178. China).p1—4

Abstract. In order to make clear the effect of the spraying technology on the coatings microstructure formation in the low pressure spraying, the wires of 4Cr13, Al and Ti were adopted to prepare the spraying coatings in air and low pressure condition, respectively. The microstructure, the amount of the compounds and their distribution pattern in both coatings were compared by the microanalysis and micro-area chemical analysis. Static press test was used to investigate the closing possibility of the porosities. After the press test, the coatings was heated to certain temperature to analyze the effect of the recrystallization heat treatment on the coatings microstructure. As a result, the amount of the oxide in 4Cr13 and Al coatings has been reduced obviously in the low pressure condition, and metallurgy combination between the splat particles can be formed by pressing and heating. However the low pressure condition can not provide sufficient protection for the Ti coatings, the following recrystallization heat treatment can not get metallurgy combination between the particles.

**Key words:** are spraying; coatings, spraying particle; oxide; recrystallization

Full digital control of I/ I mode pulsed MIG welding based on triple closed loop control

SHA Deshang, Liao Xiaozhorg (School of Automation Beijing Institute of Technology, Beijing 100081, China). p5—7, 12

Abstract: This paper presents a full digital control strategy for pulsed MIG/MAG welding based on digital signal processor (DSP) control. One droplet per one pulse (ODPP) is maintained with the proposed control strategy which is characterized by FI mode with adaptive voltage compensation (AVC). Welding database with different materials and diameters is established according to wire feed speed. Arc length is detected during each pulse period and the melting rate is charged. Moreover, real time compensation for the volt drop across the wire stickout is made to ensure the arc length constant while stickout changing. Operation principles are analyzed and control block diagram composed of triple closed loop is also presented. Experimental results show that the proposed method is feasible and universal. Constant arc length is realized when wire stickout changes. The welding process is stable and the welding bead is also good with the proposed method.

**Key words:** pulsed MIG welding; full digital control; arc length

Stereovision-based detection of 3-D weld seam using epipolar line constraint and laser stripe indication  $\mbox{ II } \mbox{Hexi}^{1,2}, \mbox{ WANG}$ 

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Abstract An epipolar line constraint equation is established for a binocolar stereovision system mounted at the end-effector of welding robot. The stereovision correspondence technique based on the combination of epipolar line constraint with laser stripe indication is applied to detect the position of a three-dimensional (3-D) saddleshaped weld seam which is produced by the intersection of two circular pipes. The experimental results show that the smooth segments of laser stripe in the weld seam image can be obtained using thinning and deburing arithmetics, and the stereovision correspondences between pairs of points at the left and the right images can be dependably realized by detecting both the singular points of laser stripe curvature and the intersecting points of laser stripe with epipolar line, thus, the detection accuracy to the 3-D weld seam and its adjacent area can be improved. The geometrical shape of the 3-D weld seam is reconstructed from the 3-D data acquired by stereovision-based detection with less errors compared with its actual dimension, therefore the proposed method can satisfy the detection regiment of 3-D weld seam in automatic robot welding system.

**Key words:** stereovision; epipolar line constraint; laser stripe indication; correspondence; weld seam detection

Plasma component calculation in underwater wet welding LI Zhigang. ZHANG Hua, JIA Jianping (Institute of Mechatronics Engineering, Nanchang University, Nanchang 330031, China). p13—16

**Abstract** The electric arc is formed in the ionized gas bubble in the underwater wet welding. Combined with the previous bubbles components determination, the main ionization and dissociation process in the bubble are analyzed. The calculation based on the potapov model was done for the underwater arc components at different water pressures and temperatures under the local thermodynamics equilibrium state. Its main theorical bases are the Dalton law of partial pressure, the law of mass action, the electric charge quasi-neutrality condition and the chemistry measurement equilibrium condition. The results show that with the pressure increasing from 0.101 3 MPa to 1.013 MPa and then to 10.13 MPa, the density of H, H<sup>+</sup>, O, C, O<sup>+</sup>, C<sup>+</sup> is increased, but the average ionization degree is not influenced by the water pressure.

**Key words:** underwater wet welding; electric arc; components calculation

Recognition and positioning of start welding position for arc welding robot CHEN Xizhang<sup>1</sup>, CHEN Shanben<sup>2</sup>(1. School of Material Science and Engineering, Jiangsu University, Zhenjiang